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Сору #

OPTICAL TECHNOLOGY DIVISION

PROJECT MEMORANDUM

PM-1519-X

19 AUGUST 1974

SENSOR SYSTEM POST FLIGHT REPORT

SV-8 (S/N 011)

Prepared by:

Flight Operations and Evaluation Section

Reviewed by:

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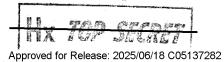
Approved by:

W.C. COTTRELL, Manager Field Operations Department

PROJECT MEMORANDUM NUMBER:	PM-1519-X
PREPARED BY;	Flight Operations & Evaluation
DATE:	19 AUGUST 1974
SUBJECT:	Sensor System Post Flight Report SV-8 (S/N OII)
DISTRIBUTION:	SP-7 (2) Maj. Berganinni) WCFO (2) SSC/DCO R. Jones W. Keeney J. Garrish P. Petty C. Karatzas L. Weeks
ABSTRACT:	This report outlines the flight history for the SV-8 (S/N OII) Sensor System.
DESCRIPTORS:	Flight Report, S/N 011 Flight Operations, S/N 011

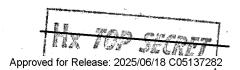
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MISSION 1208

SENSOR SYSTEM OPERATION

POST FLIGHT REPORT

1.0 INTRODUCTION

1.1 Mission Objective

The primary objective of the Hexagon Mission is to provide high resolution photography. The intent of the eighth flight was to demonstrate functional operation of the primary satellite vehicle 93 day capability. This objective was surpassed with an active mission life of 105 days.

1.2 <u>Mission Description</u>

The Hexagon Mission 1208 satellite vehicle was launched from VAFB, SLC-4E, at 1320PST 10 April 1974 using a Titan 3p booster vehicle. The first recovery vehicle was successfully retrieved from the water and the remaining three recovery vehicles were successfully air retrieved within predicted impact dispersions. Recoveries were Day 14, 42, 69 and 105 respectively.

During testing at the launch base, a small leak was detected in the fwd camera pneumatics. The leak was determined to be between the high pressure isolation valve (HPIV) and the regulator. To prevent any loss of nitrogen gas during the mission it was decided to operate with the HPIV-A closed. The count down and launch phase were accomplished without incident. After insertion, the sensor system was successfully uncaged. The constant velocity test on Rev 2 and the health check on Rev 4 were also accomplished successfully.

Operational photography began on Rev 5, Mission Op No. 4, and continued with no camera system malfunctions until Rev 980 when the system failed to execute two operations. The failure was determined to be a missing forward camera take-up Builder Roller (BR) down verification interlock signal. Operations were resumed on Rev 996 with the system configured in SCC II with BR down verification interlock disabled (VIA-DIS). When transfer to RV-4 was made, VIA was re-enabled and operated satisfactorily for the remaining portion of the mission.

IL TOP SERVET

With subsequent Vendor data the nitrogen gas leak, detected on the pad, was isolated to the low pressure side of the regulator and calculations showed the magnitude of the leak would not cause any significant increase in gas usage rate. On Rev 563 the HPIV-A was opened and the pneumatics system remained in it's normal configuration for the remaining portion of the mission.

On Rev 1268 the system shut down due to a failure of the aft camera take-up integrator servo to reset at TU brakes off. This failure necessitated eliminating nested operations when operations were resumed on Rev 1300. The system continued to operate normally for the rest of the mission.

Evaluation of the RV-I film indicated a need to change the forward camera focal plane plus 8 microns and the aft camera in-track OOAA setting minus 3 steps. These changes were made on mission ops 156 and 160 respectively. Evaluation of the RV-2 film indicated a need to change the forward camera cross-track OOAA bias by plus I step. This change was accomplished on mission OP 399.

The aft camera film supply contained one 2600 foot segment of SO-255 color film and one 3000 foot segment of FE-3916 IR color film. The operational intervals associated with the color films were as follows:

SO-255 OPS 723 to 747 Revs [51] to 1596 FE-3916 OPS 748 to 774 Revs [597 to 1694

The active photographic mission was terminated with RV-4 recovery on day 105 following depletion of both film supplies. A solo phase of the mission extended the vehicle life to day 109, at which time the vehicle was deboosted and re-entered.

1.3 Mission Highlights

Sensor system highlights of the mission can be summarized as follows:

- The sensor system demonstrated a functional orbital life of 105 days.
- b. Both forward and aft cameras utilized 100% of their respecedive film supplies. Approximately 95% of the available pneumatics was expended.



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1.3 Mission Highlights - Cont'd.

c. The sensor system demonstrated the capability to operate satisfactorily with FE-3916 infrared color film and SO-255 color film in the aft camera.

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e. The general over-all mission image quality for both cameras ranged from very good to poor; the poor being attributable to atmospheric conditions, high sun angles and specular/shadowless acquisitions. Majority of the good imagery was associated with the aft camera.

Figure I-I presents a graphic history of remaining system life percentages throughout the mission.

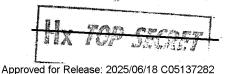
1.4 Launch Configuration

- a. Mission Operation Number 1208.
- b. Intra-range Operation No. 6245.
- c. Satellife Vehicle SV-8.
- d. Sensor System S/N Oll.
- e. Sensor System Configuration.

	Forward Camera	Aft Camera
Filter Types	W-12	W-12
Focal Length	59.9760 in.	59.9890 in.
Focus Setting	68 Microns	25 Microns
OOAA Setting		
In-Track	-4 CMD Steps	-2 CMD Steps
Cross-Track	I CMD Step	-3 CMD Steps
Film Type	1414	1414/S0-255/FE-3916
Film Length	108,854	106,567
Film Weight	862.1 lbs.	861.4 lbs.
Spool Number	5077	5076
Pneumatics Loaded	35.4 lbs	•

1.5 Launch and Orbital Parameters

	Planned	<u>Actual</u>
Launch Time-GMT	2020Z	2020Z
Launch Time-SVT	67.0	67.0
Inclination-degrees	94.51	94.52



1.5 Launch and Orbital Parameters-Cont'd.

	Planned	<u>Actual</u>
Initial Perigee-n. miles	84.94	85.55
Initial Apogee-n. miles	162.22	164.73
Argument of Perigee-		
degrees	149.71	141.36
Initial Period-minutes	89.0	89.01

Table 1-1 and Figures 1-2 and 1-3 define the basic orbital parameter considerations for the active mission. Forty-three orbit adjusts were performed.

1.6 Mission Film Usage Summary

The distribution of film footage as functions of the various operating modes is presented in Figures I-4 to I-21. The mission segment to segment film usage is summarized as follows:

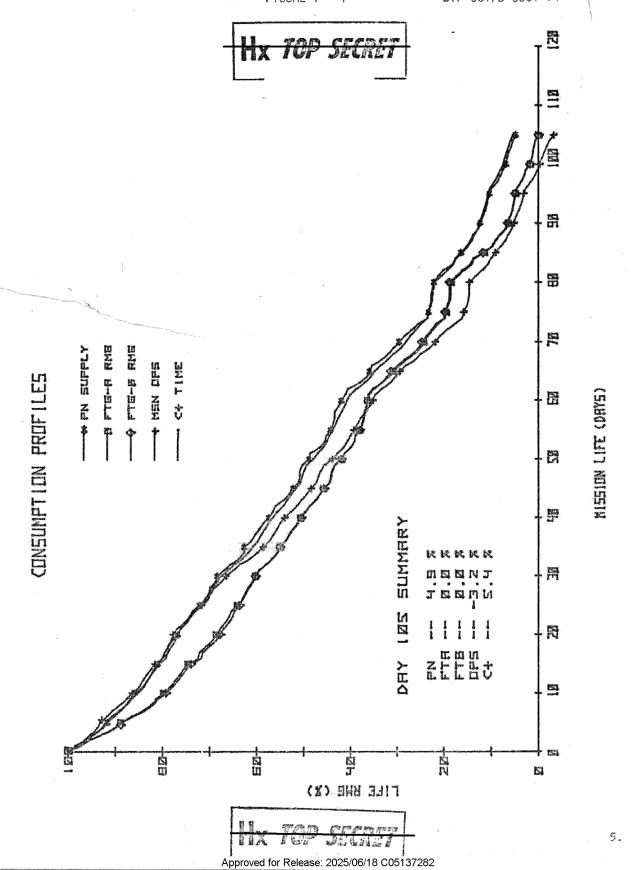
·	Rev Span	Camera	Recovered Footage
RV-I	Launch-225	Forward Aft	28042 28111
RV-2	226-674	Forward Aft	28848 27766
RV-3	675-1116	Forward Aft	25258 24225
RV-4	1117-1700	Forward Aft	26827 26608

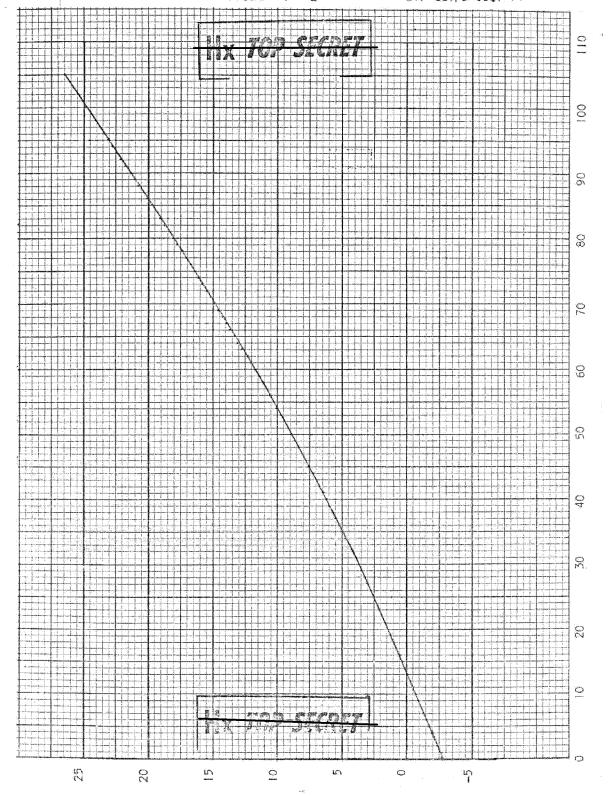
Of this footage, the engineering and other non-intelligence operations consumed approximately 4600 and 4800 feet for the A and B sides, respectively, as summarized in the following:

IZU8 Non-	-Intelligence	
	Forward Camera	Aft Camera
Pre-Launch	1853	1991
RV-I Engineering	1055	1055
RV-2 Engineering	702	702
RV-3 Engineering	437	478
RV-4 Engineering	596	605
Total Utilization	4643	4831
FIIm Recovered	108975	106710
PCT. Non-Intelligence	4.26	4.53

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4.





BETA ANGLE (DEGREES)

| S X S TO THE CENTIMETER IS X 24 CM. KEUFFEL & ESSER CO.

FIGURE 1 - 3

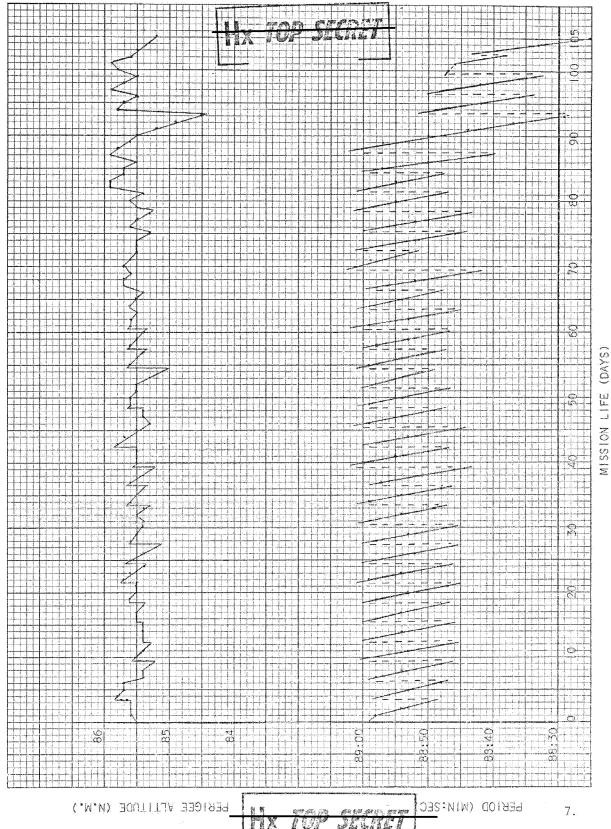


TABLE I - I

BASIC ORBITAL PARAMETERS

DAY	REV	PERIOD	PERIGEE	APOGEE	TNC	ARG/PER	B ANG
0 0 1 2 3	NOM 1 8 24 40	88:59 89:00 88:58 88:54 88:50	85.5 85.6 85.6 85.6	162.9 164.5 163.5 161.0 158.4	94.5 94.5 94.5 94.5 94.5	143.4 141.0 138.9 134.8 130.6	-2.6 -2.6 -2.3 -2.1
OA#1 4 5 6 OA#2 OA#3	46 57 73 89 94 96	88:57 88:53 88:48	85.8 85.7 85.7	165.1 162.7 160.1	94.5 94.5 94.5	130.9 126.7 122.7	-1.9 -1.7 -1.5
7 8 9 0A#4	105 121 138 143	88:58 88:54 88:48	85.4 85.4 85.3	161.1 158.5 155.0	94.5 94.5 94.5	147.5 143.2 138.4	-1.3 -1.1 -0.9
10 11 12 0A#5	156 170 186 192	88:58 88:53 88:47	85.5 85.4 85.3	162.4 159.5 156.5	94.5 94.5 94.5	132.0	-0.7 -0.5 -0.3
13 14 15 0A#6 0A#7	202 218 235 240 242	88:58 88:54 88:48	85.4 85.4 85.4	165.4 162.5 159.1	94.5 94.5 94.5	133.9 129.8 125.3	-0.1 +0.1 +0.3
16 17 18 0A#8	251 267 283 289	88:58 88:54 88:49	85.5 85.5 85.4	160.7 158.0 155.2	94.5 94.5 94.5	147.2 143.0 138.8	0.5 0.8 1.0
19 20 21 0A#9	299 313 332 337	88:58 88:53 88:47	85.6 85.5 85.5	162.7 160.2 156.3	94.5 94.5 94.5	140.1 135.5 131.2	1.2 1.4 1.6
22 23 24 0A#10 0A#11	348 364 380 386 388	88:59 88:54 88:48	85.7 85.6 85.4	166.2 163.1 159.5	94.5 94.5 94.5	133.4 129.6 125.5	1.9 2.1 2.3
25 26 27 OA#12	397 413 429 434	88:58 88:52 88:47	85.6 85.4 85.2	160.3 157.2 154.2	94.5 94.5 94.5	147.2 142.8 138.4	2.5 2.7 3.0

TABLE i - 1 Cont'd.

BASIC ORBITAL PARAMETERS

DAY	REV	PERIOD	PERIGEE	APOGEE	INC	ARG/PER	B ANG
28	445	88:58	85.6	162.0	94.5	141.8	3.2
29	461	88:53	85.5	159.1	94.5	137.6	3.5
30	477	88:47	85.4	155.8	94.5	133.3	3.7
OA#13	483	20.50		وست سوني ر			
31	494	88:59	85.4	165.3	94.5	135.4	3.9
32	510	88:54	85.5	162.5	94.5	131.1	4.2
33 0A#14.	526	88:49	85.4	159.5	94.5	127.0	4.4
OA#14.	532 534						
-34	542	88:59	85.6	161.0	94.5	147.9	4.7
35	558	88:54	85.5	158.3	94.5	143.5	4.9
36	575	88:48	85.4	154.6	94.5	138.8	5.2
0A#16	580	09.,0		,,,,,	£ 1.5.4.	,,,,,,	,
37	591	88:57	85.6	161.8	94.5	140.7	5.5
38	607	88:51	85.4	158.6	94.5	136.5	5.7
39	623	88:46	85.3	155.4	94.5	132.3	6.0
OA#17			*				
40	639	89:00	85.5	166.3	94.5	135.6	6.2
41	655	88:55	85.5	163.4	94.5	131.4	6.5
42	672	88:50	85.5	160.4	94.5	126.9	6.8
0A#18	683						~ .
43	688	88:58	85.8	166.6	94.5	128.3	7.0
44 45	704 720	88:53 88:46	85.7 85.5	163.3 159.5	94.5 94.5	124.3 120.4	7.3
0A#19	726 726	00:40	ر. ره	109.0	94.0	12U,4	7.6
0A#19	728						
46	736	88:59	85.3	161.9	94.5	148.5	7.8
47	753	88:54	85.4	158.7	94.5	143.6	8.1
48	769	88:49	85.4	155.7	94.5	139.2	8.4
OA#21	774			,		*	
49	785	88:59	85.6	163.0	94.5	141.1	8.6
50	805	88:49	85.6	160.1	94.5	136.9	8.9
51	817	88:48	85.5	156.6	94.5	132.7	9.2
0A#22	823						
52	834	88:58	85.5	164.9	94.5	133.8	9.5
53	850	88:52	85.3	161.3	94.5	129.6	9.8
54	866	88:51	85.1	157.7	94.5	125.5	10.1
OA#23 55	871 882	88:59	0E 6	167 6	04 5	FOO C	10.7
56	896	88:54	85.6 85.5	167.6 164.3	94.5	129.6 125.5	10.3
57	914	88:49	85.4	160.8	94.5 94.5	121.4	10.6
21	21.4	00.49	リノ・ サ	10040	24.2	121'54	10.7

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TABLE I - I Cont'd.

BASIC ORBITAL PARAMETERS

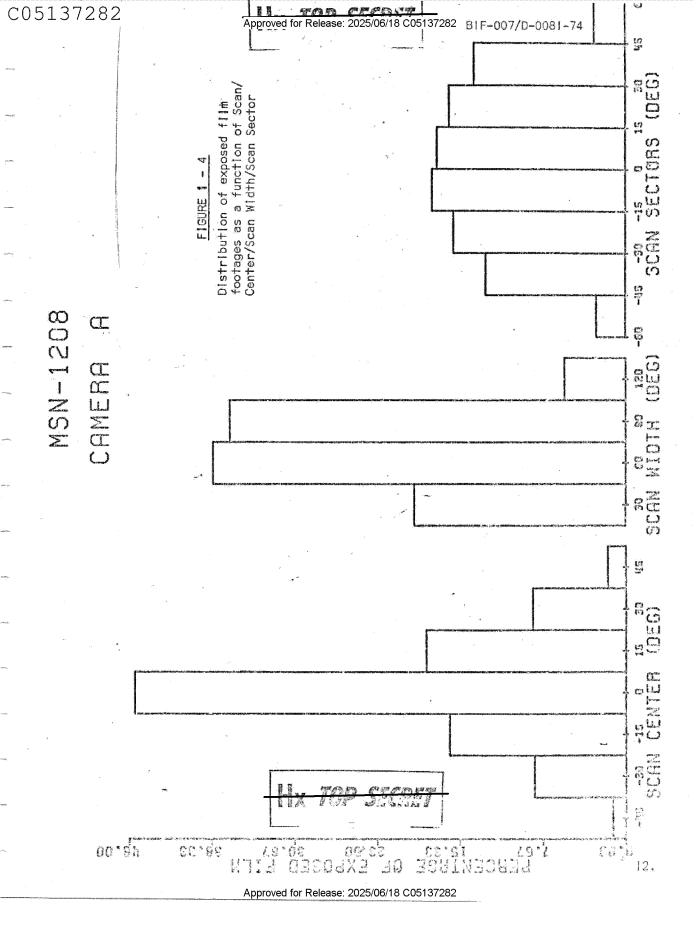
DAY	REV	PERIOD	PERIGEE	APOGEE	INC	ARG/PER	B ANG
OA#24	920						
0A#25	922						
58	931	88:58	85.6	160.6	94.5	147.6	11.2
59	947	88:53	85.5	157.8	94.5	143.1	11.5
60	963	88:48	85.4	154.9	94.5	138.7	11.8
0A#26	975	00:40	62.4	. 124+9	34.3	100.7	11.0
61	979	88:59	85.6	162.9	94.5	142.5	12.1
62	996	88:53	85.6	159.5	94.5	138.2	12.4
63	1012	88:47	85.5	155.4	94.5	133.5	12.8
OA#27	1017						
04	1029	88:59	85.6	165.5	94.5	136.4	13.1
65	1644	88:54	85.5	162.2	94.4	132.2	13.4
66	1060	88:49	85.4	158.7	94.4	128.1	13.7
OA#28	1065	The second secon	Garagea.				
67	1076	88:57	25.7	165.2	94.4	130.2	14.0
68	1092	88:52	85.7	161.7	94.4	126.1	14.3
69	1109	88:44	85.6	156.8	94.4	121.5	14.6
OA#29	1120						
70	1125	89:06	85.7	174.1	94.5	127.0	14.9
71	4	88:59	85.6	169.8	94.5	122.8	15.2
72	1157	88:53	85.5	165.9	94.4	118.9	15.5
OA#30	1162						
0A#31	1164						
73	1173	88:58	85.5	160.2	94.4	147.7	15.9
74	1190	88:52	85.5	157.0	94.4	143.0	16.2
75	1206	88:46	85.3	153.5	94.4	138.5	16.5
OA#32	1211						1
76	1222	88:57	85.6	161.8	94.4	141.1	16.8
77	1238	88:52	85.5	158.7	94.4	137.0	17.1
78	1254	88:45	85.3	154.1	94.4	132.8	17.4
OA#33	1260		,	عد والد و	20.4 20		170
79	1270	88:59	85.5	164.9	94.4	137.5	17.8
OA#34	1282	00 55	25.6	وسيدر و	:0. 4 A	1774	10.1
80	1286	88:55	85.6	162.3	94.4	134.1	18.1
81	1303	88:49	85.4	158.5	94.4	129.9	18.4
0A#35	1313	00.50	DE A	1000	0.4.4	177 0	10.0
82 83	1321	88:59 88:55	85.9	166.2	94.4	133.0	18.8
84	1335 1351	88:49	85.9 85.7	163.3 159.5	94.4 94.4	129.3 125.2	19.1
0A#36	1357	90:47	02.7	158.5	94.4	122.2	17.4
85	1368	88:57	85.7	167.3	94.4	125.9	19.8
0.5	1200	00273	N.J F.	107,5	2™ • **	147.3	19.0

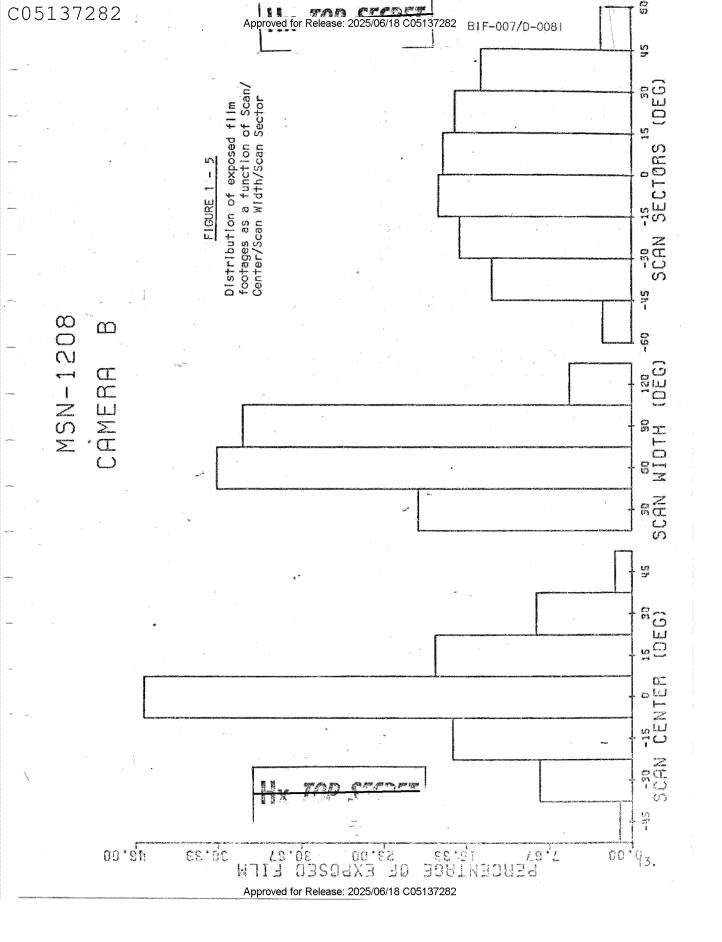
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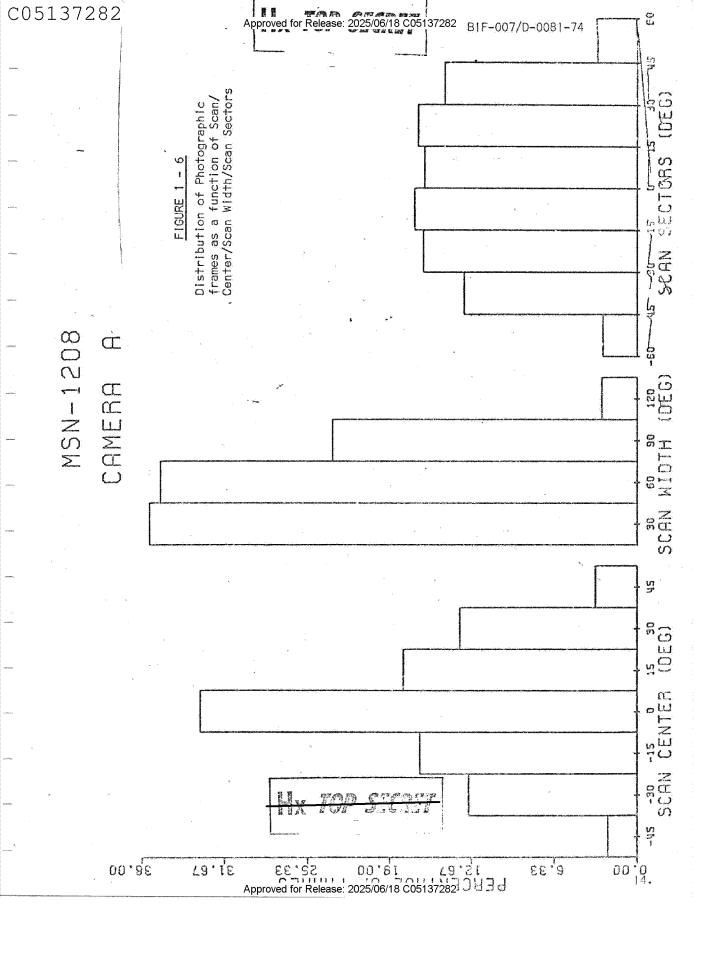
TABLE I - I Cont'd.

BASIC ORBITAL PARAMETERS

	DAY	REV	PERIOD	PERIGEE	APOGEE	INC	ARG/PER	B ANG
	86	1384	88:50	85.5	162.8	94.4	121.8	20.1
	87	1400	88:42	84.9	156.8	94.4	117.6	20.4
	0A#37	1406	00.42	04.3	120.0	24.4	117.0	20.4
	OA#38	1408						
	88	1416	89:02	85.8	164.3	94.4	148.0	20.8
	89	1432	88:57	85.6	160.7	94.4	143.6	21.1
	90	1449	88:50	85.5	156.3	94.4	138.0	21.4
			88:44			94.4		21.8
	91	1465		85.2	152.3		134.4	
	al Ka	1481	88:37	84.9	147.8	94.4	129.9	22.1
	93	1497	88:29	84.5	142.9	94.4	125.5	22.4
	OA#39	1502	20.45	AL 200 PA	100	~	170.0	no n
	94	1513	88:49	85.8	155.1	94.4	138.0	22.8
	95	1530	88:42	85.7	151.2	94.4	133.2	23.1
	96	1546	88:36	85.5	147.2	94.4	128.8	23.4
	OA#40	1551	F					
	97	1562	88:48	85.9	155.1	94.4	134.3	23.8
	98	1578	88:42	85.7	151.3	94.4	130.0	24.1
	99.	1594	88:35	85.5	147.2	94.4	125.7	24.4
1	OA#41	1600						
	100	1611	88:47	85.8	156.1	94.4	130.3	24.8
	OA#42	1616						
	101	1627	88:46	85.9	155.6	94.4	128.6	25.1
	102	1643	88:39	85.6	151.8	94.4	124.6	25.4
	OA#43	1649						
	103	1659	88:41	85.5	153.1	94.4	123.9	25.8
	104	1676	88:33	85.2	148.3	94.4	119.3	26.1
	105	1692	88:24	84.3	141.4	94.4	115.0	26.5







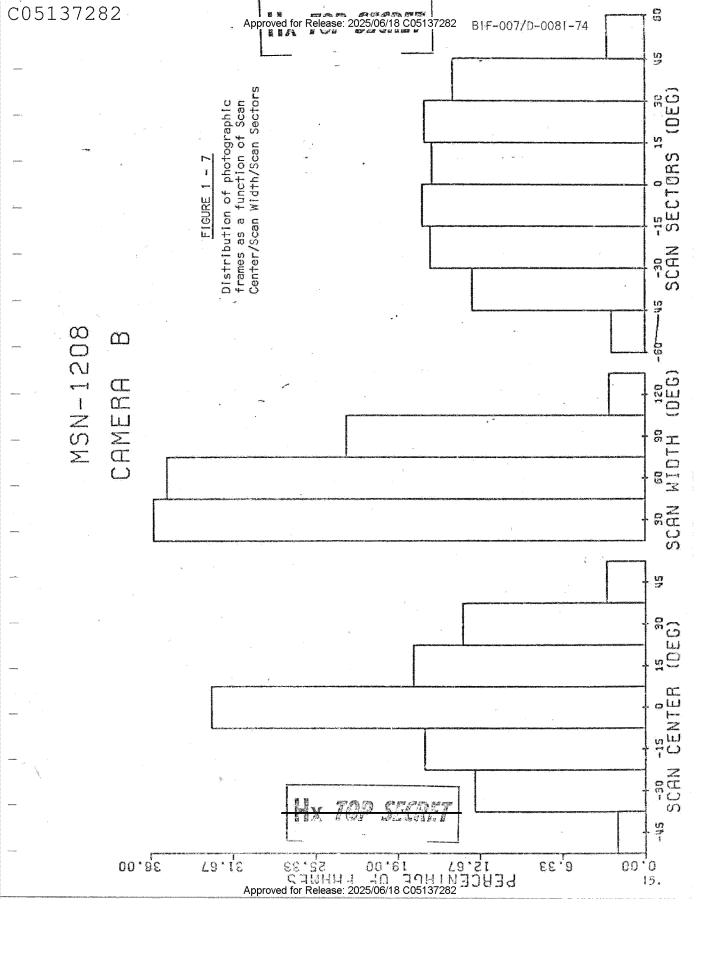


FIGURE 1 - 8

Distribution of land mass coverage as a function of Scan Sectors



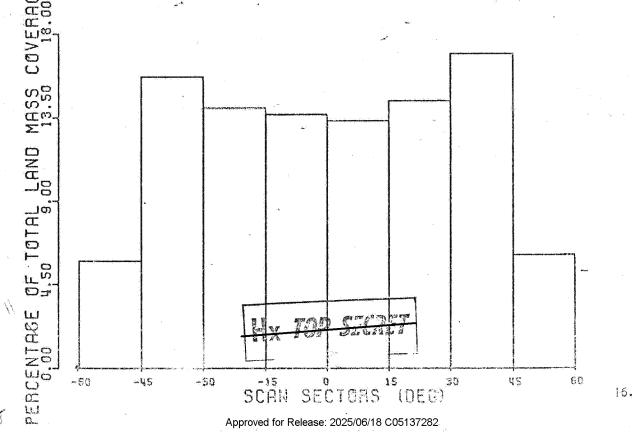
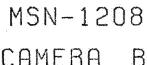
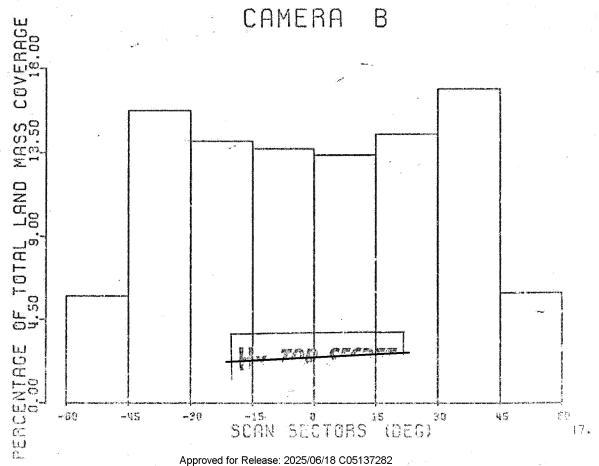
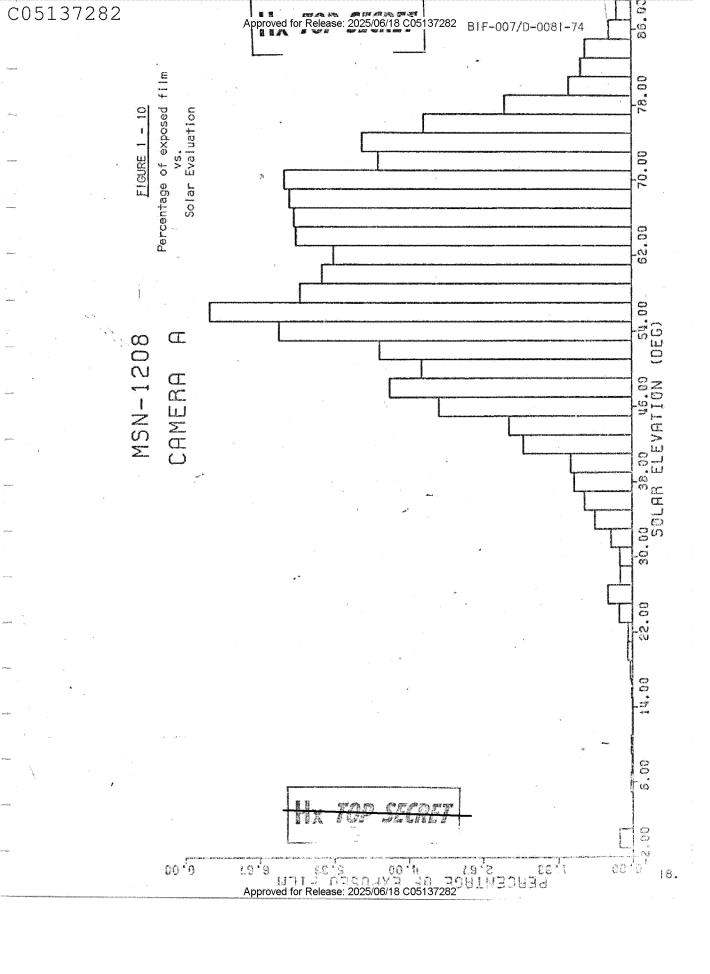


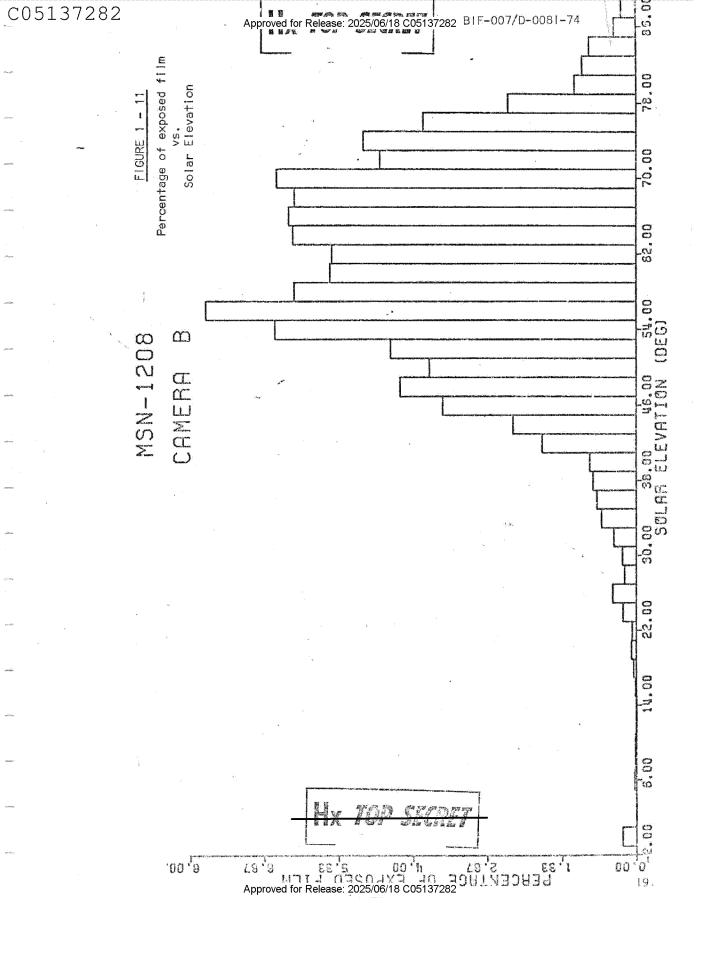
FIGURE 1 - 9

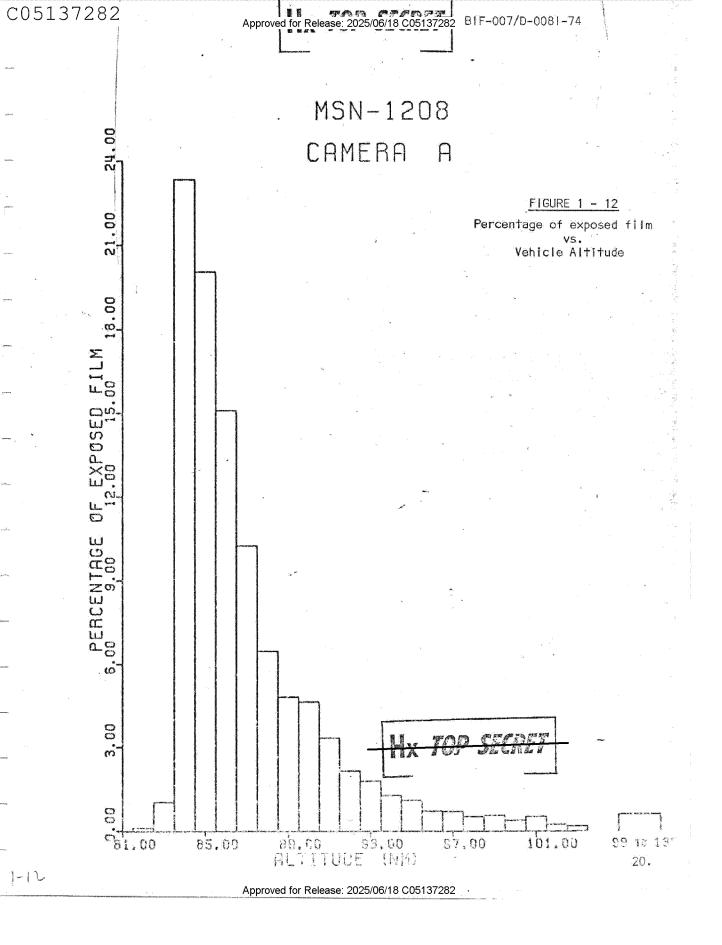
Distribution of land mass coverage as a function of Scan Sectors

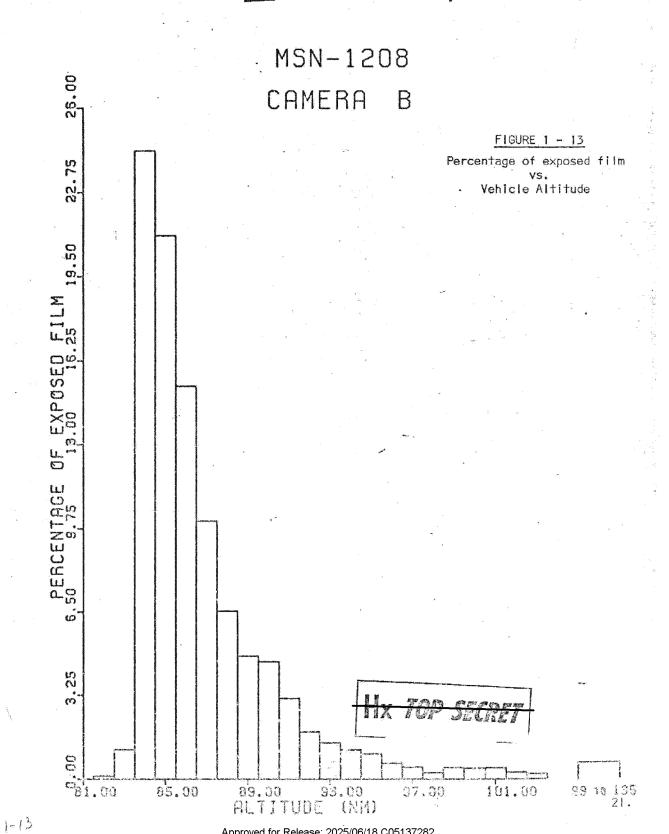












15.75

13.50

OF EXPOSED FILM 9.00

PERCENTAGE

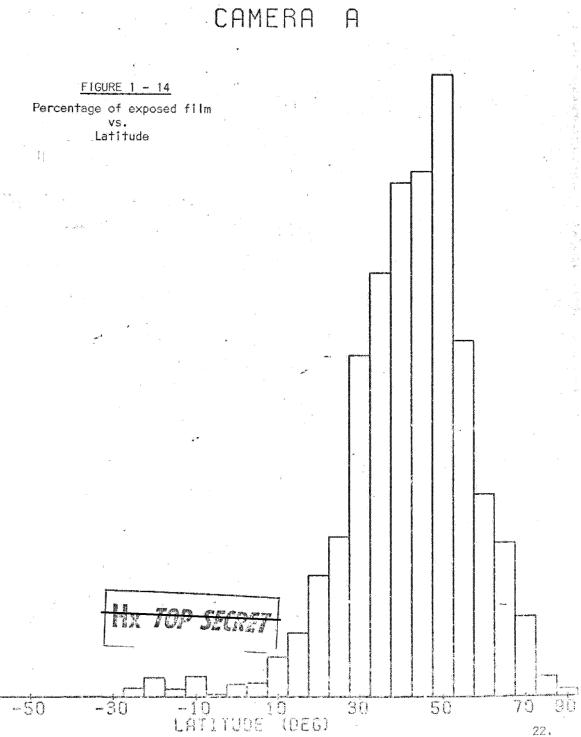
2.23

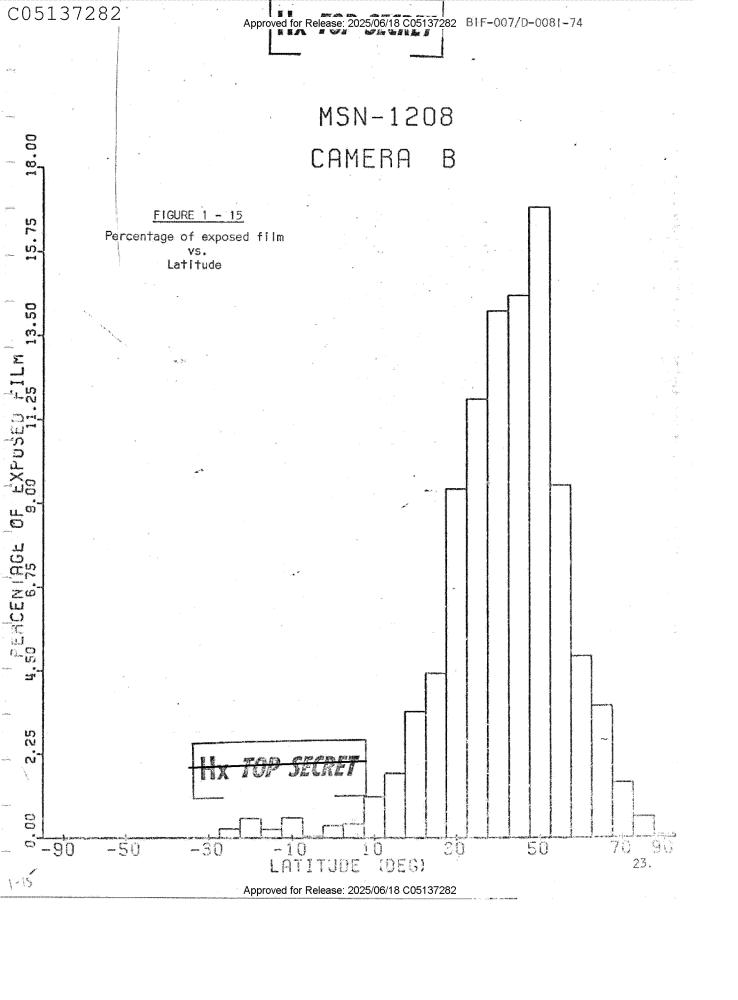
0.00

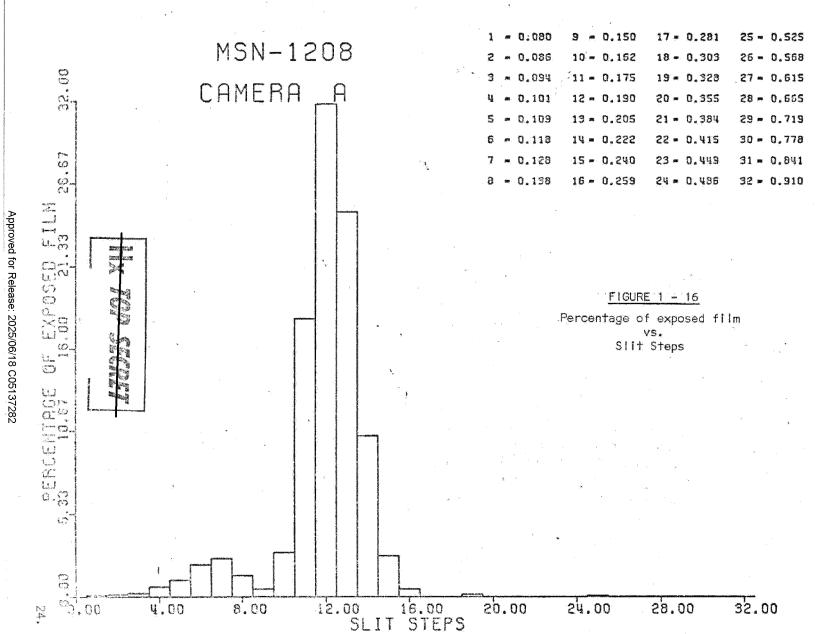
1-1-

-90









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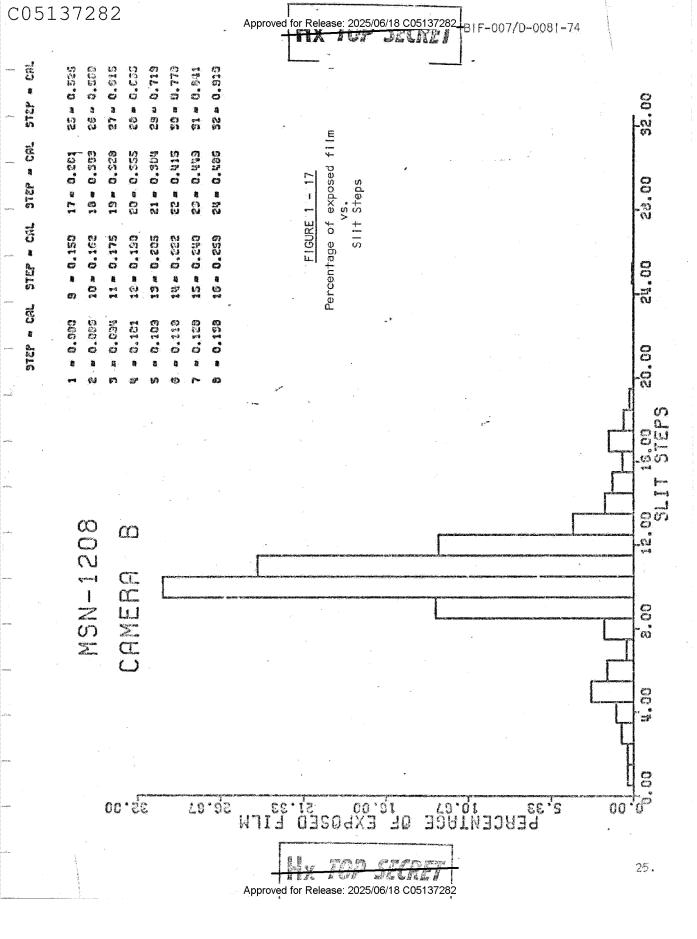
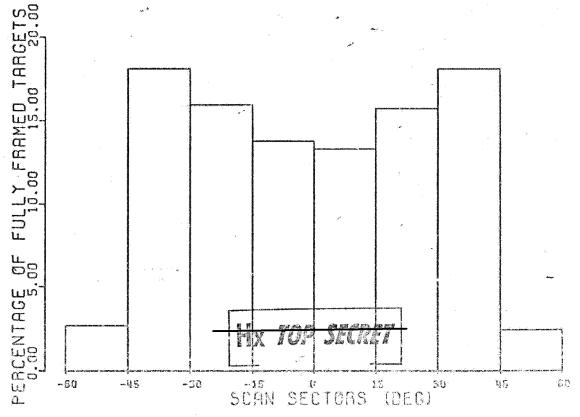


FIGURE 1 - 18

Distribution of fully framed Targets vs. Scan Sectors

MSN-1208 CAMERA A



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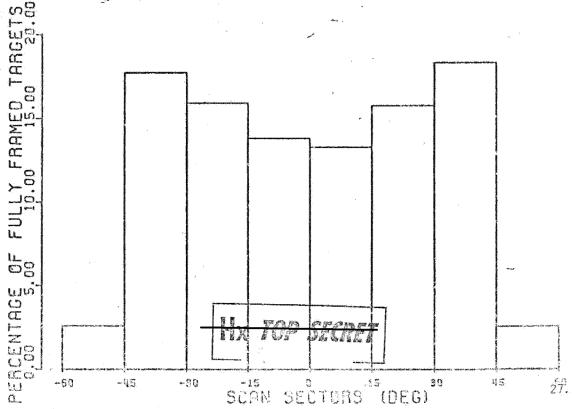
26.

1-19.

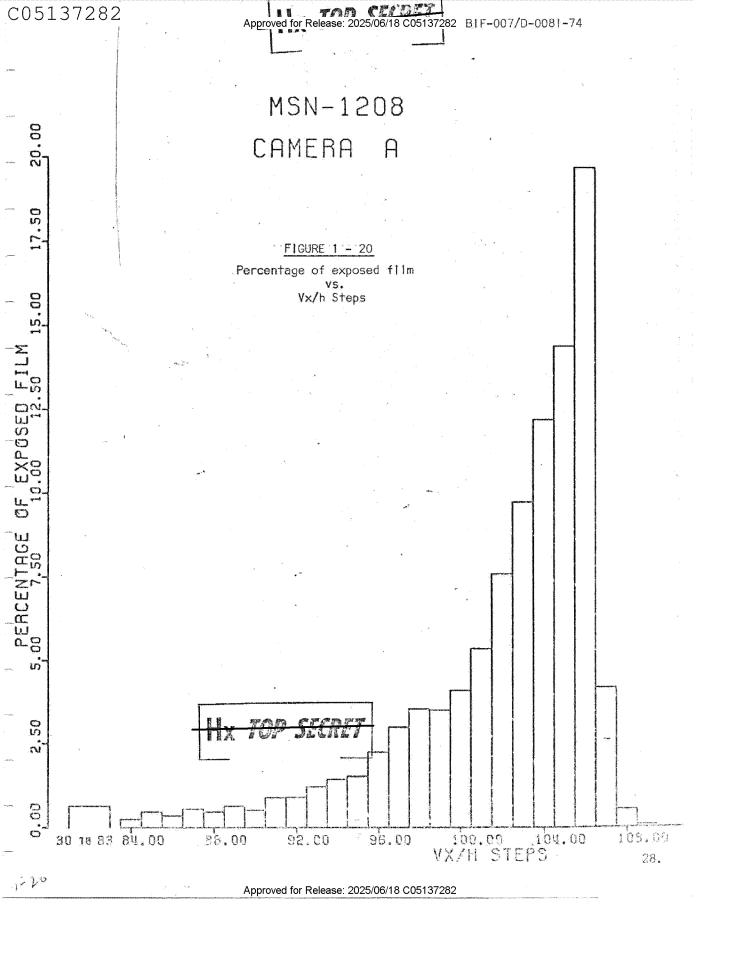
FIGURE 1 - 19

Distribution of fully framed Targets vs. Scan Centers

MSN-1208 CAMERA B



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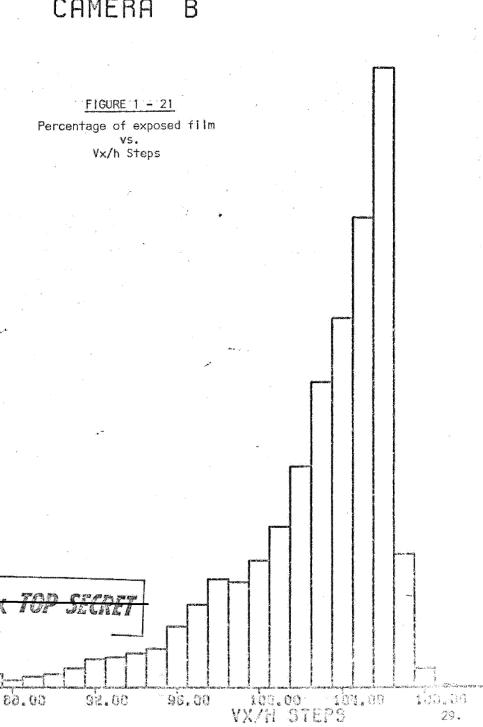


(S)

S. SO PENCENTHGE OF EXPUSED FILM

30 to 82 84.00

MSN-1208 CAMERA B



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2.0 SENSOR SYSTEM PERFORMANCE

2.1. Coarse Film Path

Coarse film path diagnostics indicated nominal performance throughout take-ups one, two and three. Analysis of a B-side emergency shut down (ESDB), which occurred during take-up four operations, indicated a hardware failure in the coarse path control electronics.

The ESDB occurred on the start-up of an operation planned for Rev 1268 and was due to a low tension condition in the coarse path. A B-side creep test conducted over 1283 Pogo also shut down, but this shutdown was due to a high tension coarse path condition.

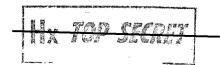
Analysis of the Rev 1268 ESDB and primarily of the Rev 1283 ESDB indicated that the take-up integrator reset signal to the take-up servo loop was not operating. The Rev 1268 data was in telemetry mode C, as is most operational payload data, and the take-up integrator output signal is not included in the telemetry format. The Rev 1283 data was in telemetry mode B which does include the take-up integrator output signal.

The take-up integrator integrates the output coarse tension error from nominal and modifies the take-up servo error signal, which is also a function of the velocity command, velocity feedback and the coarse output tension offset. The take-up servo responds by altering the take-up velocity in a manner consistent with correcting the output coarse tension error.

Integration of the tension error begins at camera power turn-on. There is a small tension error at the start-up of most camera operations, and because of the nominal time delay between camera power on (CB+) and film transparts on (FT+), the integrator out-put at the time the take-up brakes are released can be substantial. Therefore, the integrator output is reset to null upon application of brake release power via the 35ms. reset signal generated within the take-up electronics.

In the absence of the reset signal, the integrator output will erroneously alter the error signal to the servo loop. The magnitude of the error introduced is dependent on the original coarse output tension offset and the time duration between camera power on and transports on.

In the case of the Rev 1268 ESDB, the CB+ to FT+ time was in excess of 120 seconds for film path pressurization purposes, and although the initial coarse tension offset was small, the integrator output was saturated by the time brakes released and indicative



of a much larger over tension condition than what actually existed. The servo loop therefore overcorrected for the actual tension error and subsequently caused the under tension ESDB. The Rev 1283 ESDB resulted when the servo overcorrected for an initial undertension condition and drove the system into the high tension state.

Analysis of coarse tension data from currently available station tapes indicated integrator failure occurred between operations 598 and 605. Under normal operating conditions (i.e. initial coarse output tension greater than 2.2 lbs. and less than 2.8 lbs; CB+ to FT+ less than or equal to 17 seconds) the TU servo can recover from the integrator error present at brake release without the reset signal. The remainder of take-up four operations were constrained to a maximum C+ to FT+ time of 17 seconds and the startup coarse output tension limits noted above. No further problems in this area were encountered.

2.2 Fine Film Path

Fine film path diagnostics indicated proper hardware performance throughout the mission for both camera systems.

2.3 Command and Control

The sensor system performance with respect to the Command and Control Subsystem was nominal throughout the mission. All commands were properly received and executed.

2.4 Sensor System Control

On Rev 980 the sensor system failed to execute the second and third of three non-nested operations. The first operation, Msn OP 490, executed normally.

The set-up commands for the two Ops that failed to execute, up to and including seal doors open, were properly executed. Neither the SU nor the TU brakes were released and the film transports did not operate.

On Rev 989 both an A-Side and a B-Side CV test were run with verification interlocks enabled. The A-Side test failed to execute. The B-Side test executed normally. On Rev 991 an A-Side CV test was successfully executed with verification interlocks disabled.



On Rev 993 an A-Side CV test was run with SCC-II and verification interlocks disabled. This test also failed to execute which isolated the problem to the A-Side verification circuitry external to either SCC | or SCC | II. The most probable suspect for the failure was an absence of the "Builder Roller Down" verify signal.

On Rev 995 a health check was successfully executed in SCC II with VIA disabled. Stereo operations were resumed on Rev 996 using SCC II with VIA disabled and continued without further problems through the remainder of RV-3.

When transfer to RV-4 was made, VIA was re-enabled and the mission successfully completed in that configuration with SCC II.

Upon receipt of the RV at Rochester, the outer shrouds were removed and a visual inspection was made with an infrared scope and infrared photographs were taken. Both the visual inspection and the photographs indicated that the condition of all portions of the Builder Roller and the lower verify switch were normal. Extensive electromechanical testing did not provide any information to help isolate the cause of the Builder Roller Verify signal failure.

2.5 Optical Bar Performance

The Optical Bars performed properly throughout the mission. Variations between commanded and actual OB velocities were no different than those noted during pre-flight systems test and were within the specification limits of .00054 rad/sec.

2.6 LSFS/Focus

Mission 1208 used pre-flight determined focus settings for 1414 black and white film, SO-255 color film and FE-3916 infrared film.

The forward camera was set at a nominal of 68 microns through RV-1. Image quality evaluation of the returned film resulted in a change to a new nominal of 76 microns commencing with Msn Op 156 in RV-2 and continuing through the remainder of the mission.

The aft camera was set to a nominal of 25 microns for 1414 material and 55 microns for both SO-255 and FE-3916. No readjustments from the pre-flight planned values were required.

The LSFS output, as with 1207, was deemed reliable only on the first operation of each day (i.e., after three hours of non-operation and during the first five minutes of the first subsequent OP). Readings of the LSFS output were taken only at these times throughout mission 1208.



32.

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2.7 Instrumentation

All instrumentation operated normally throughout the mission. The system provided consistent and accurate data for analysis of anomaly conditions and for the routine verification of camera status. Although not part of the sensor system instrumentation system, a MUX failure necessitated switching from the primary (MUX 4A) to the backup (MUX 4B) unit.

2.8 Pneumatics

The pneumatic system nitrogen reserve status for mission 1208 was as follows:

		TANK		TANK B			
Even†	Press. (psi)	Temp (°f)	Mass (lbs)	Press (ps1)	Temp (°f)	Mass (lbs)	Total Mass (Ibs)
Liftoff	3388	69	17.8	3374	68	17.7	35.5
End of Primary Mission	196	69	1.1	210	67	1.2	2.3

Toward the end of the mission it became necessary to manage camera operation in terms of the distribution of scan centers, scan lengths and frame count to avoid the possibility of depleting the gas supply prior to the total usage of the film supply. The computed PN+ use rate was a constant 0.023 lbs/min throughout the mission.

2.8.1 During the launch countdown, on Day R-1, the A side regulated pressure was observed to decay at an abnormally high rate, e.g., from 2.46 to 1.28 psi in 300 seconds. On the basis of this decay rate and the immediately available design data, several hundred manufacturing drawings, pertaining to the pneumatic system plumbing volumes, it was concluded that a leak had developed on the high pressure side of the regulator and was of sufficient magnitude to be unacceptable for flight operation, i.e., the continuous loss of gas would severely shorten the mission. An acceptable corrective action was taken by isolating the leak from the high pressure gas supply, tank pressure, by commanding the A side high pressure isolation valve (HPIV-A) to the closed position following the uncage and OB stow sequences executed on Rev 0. The only disadvantage to this configuration was a reduction in system reliability as a result of the loss of parallel redundancy in the D bar gas supply.



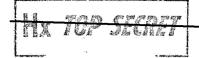
Subsequent to the launch, the plumbing system volumes were measured at the supplier's facility and determined to be significantly different from the values calculated from drawings. (The measured values were: high pressure stage = 0.290in³, intermediate pressure stage = 0.036in³, low pressure stage = 3.085in³.) New analysis were performed and it was concluded that the leak was on the low pressure side of the regulator and was of negligible magnitude. Therefore, it was decided to open the HPIV-A to regain maximum system reliability.

As a precaution, on orbit tests were performed to verify that the leak was in the low pressure stage. The tests were conducted by momentarily opening the HPIV-A and monitoring the regulated pressure decay rate following valve closure. As a result of the analysis and tests, the HPIV-A was opened on Rev 563 and left open for the remainder of the mission.

A detailed analysis of the pneumatics system leak is provided in, "Memorandum #930, OTD, SED, SAE, To: C. Karatzas, From: H. Yanowitz and B.E. Nelson", dated: 2 May 1974.

2.8.2 Path Pressurization

For the first time in eight missions it became necessary to acuate the pneumatic system operate valves to maintain the film path pressure above the ballooning criterion. The initial repressurization occurred after transfer to TU-4 and was repeated as required for the remainder of the mission. Although the path leak rate was within specification requirements, the combination of short operations with corresponding small increases in path pressure, separated by long quiescent periods caused the repeated occurrence of the low pressure condition. To minimize the additional gas usage, a procedure was used wherein the path was repressurized, increased by approximately 0.1 psi, only at those times the path pressure had decayed to the ballooning pressure limit.



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2.9 Tr

Trend Analysis

A statistical trend analysis of sensor system performance was maintained by the Systems Integration Section throughout mission 1208. Data samples were taken from one operation per day, when available, and mean values and standard deviations were calculated and plotted for selected functions to facilitate the detection of any long term trands that would indicate the orbit of system degradation. The analysis indicated a momentary disturbance in all tension sensors and the A side metering capstan summed error in the first 12 scan degrees of operation 564, however, the signals returned to nominal values for the remainder of the operation. Although not regarded as a trend or anomaly, the B side metering capstan summed error mean valve shifted from 0.034 oz. in. with 1414 material to approximately 0.043 oz. in. with \$0-255 film. The mean level returned to approximately 0.034 oz. in. with FE3916 film. Otherwise, all system functions remained nominal throughout the mission with no indication of abnormal long term trend.

The functional parameters used for the analysis were as follows:

- 1. Film to Bar Sync Velocity Error (P451, P452)
- 2. Metering Capstan Summed Error (P403, P404)
- 3. Platen Skew Error (P415, P416)
- 4. Platen Photo Summer Error (P411, P412)
- 5. Input Drive Capstan Summed Error (P803, P804)
- 6. Output Drive Capstan Summed Error (P811, P812)
- 7. Supply Drive Summed Error (P105, P106)
- 8. Take-up in Use Drive Summed Error (TSEA, TSEB)
- 9. Optical Bar Summed Error (P501, P502)
- 10. OB Velocity Error
- 11. Looper Position (P601, P602)
- 12. Film Path Carriage Position (P713, P714)
- 13. Take-up Carriage Position (P951, P952)



3.0 MISSION EVENT HISTORY

A summary listing of all sensor system photographic operations is presented in Appendix A-I of this report. The summary primarily covers operational photography, but also includes SS and PFA engineering photography. The following is a chronological description of these engineering operations plus other special events that occurred during Mission 1208.

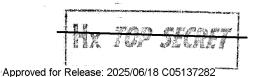
3.1 Ascent

The countdown and launch were accomplished without incident, with uncage (sequences 204 and 205) and OB stow (sequences 213 and 214) occurring in a normal manner following BV-SV separation. These events were verified from tape recorder playback at Rev 1 POGO.

3.2 Health Checks

Day I operations through Rev 4 were designed to verify system health and confirm orbit operational readiness. An engineering operation designed as a baseline test was performed on Rev 8. The health check events were as follows:

- Rev I: An uncage verification check, sequence 215, was performed over POGO to confirm the uncage event.
- Rev 2: A constant velocity run, sequence 208, was performed over KODI. This was the first attempt to transport film after launch. The Sensor System worked properly, and the film was correctly aligned within the film path. Steerers, tensions, and take-up and supply drive summed errors were well within limits.
- Rev 4: The sensor system health check, sequence 175, was performed over POGO. All sensor system executed commands were functionally verified, including all tested bits of the variable commands. Focal plane position indicated 68 microns for the forward camera, and 25 microns for the aft camera.
- Rev 8: A scheduled engineering operation, sequence 209, was performed over COOK to provide characteristic telemetry data for comparison with data from any future identical functional check. In the event of an anomaly, the telemetry signatures of the two runs could then be equated and any suspected system degradation determined.

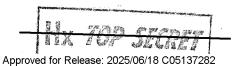




3.3 **Engineering Events**

Eleven engineering tests were defined in the SV-8 Engineering Photography Plan. This series of tests were designed to acquire data for assessment of on-orbit camera, lens and film performance. Following is a summary of the tests and their objectives:

	Test	Objective/Status
l.	Thru-Focus (1414)	Optimize Focus. Fully accomplished; confirmed focus (1414) was optimum in RV-2.
3.A	Smear Slits (1414)	Validate Image Motion Compensation settings. Completed in RV-2.
3 . B	Smear Slits (SO255)	Evaluate smear slit for validating image motion compensation settings with color film. Completed in RV-4.
3.C	Smear Slits (FE3916)	Evaluate smear slit for validating image motion compensation settings with IR film. Completed in RV-4.
4.	Color Corn Acquisitions	Evaluate and radiometrically call- brate SO-255. Satisfactorily completed in RV-4.
5.	IR Color Corn Acqui- sitions	Evaluate image quality of FE3916. Accomplished in RV-4.
6.	Lens MTF (1414)	Measure on-orbit lens MTF. Completed in RV-3.
7	Tucson Acquisition	Standard scene for quality assessment. Satisfied in RV-1,2,3 and 4.
8.	Color Thru-Focus (SO-255)	Optimize Focus. Completed in RV-4.
9.	Tri-Bars for Resolution	Photo quality assessment. Satisfied RV-1,2,3 and 4. Acquisitions common with Test 7.
10.	Smear versus Scan Angle (1414)	Assess smear as a function of scan angle location. Fully accomplished. Completed in RV-3.
12.	Dense Culture Acquisition (1414)	Photo/EM correlation. Satisfied in RV-1,2,3 and 4.



		3.4	Mission	1208-1 5	pecial E	Events	the state of the s		
			REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
			0.8				UNCAGE/SCC I SEL		
· ,	٧		0.8				STOW A/STOW B HPIV A CLOSE		
√pprov	1	3	1				UNCAGE VERIFY		
ed for			2				INHIBITED CV		102
Relea			4	1-3			SS HEALTH CHECK		163
lse: 20			8	8			SS ENGINEERING		63
Approved for Release: 2025/06/18 C05137282			14	13	Service .	75 75	1414 T/F-8,-16,-8,0,+8,0 BOSTON PROVIDENCE	99 99	. 54
05137282	3		16	14	1	95	1414 T/F +16,+8,0 SAN DIEGO	90	29
10 ====			56	42			PN EQUALIZE		
			81	54	and the second	85 80	1414 T/F-16,-8,0 SACRAMENTO SAN FRANCISCO	95 99	56
			86	55			PN EQUALIZE		
			96	63	3A	70	1414 SMEAR SLITS DALLAS/FT WORTH	99	81

1055

Mission 1208-1 Special Events-Cont'd. 3.4

		REV	OFN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
		97	64	3A.	95	1414 SMEAR SLITS LOS ANGELES	99	
				10	85	1414 SMEAR VS SCAN SAN DIEGO	99	124
ta goas		129	84	7,9,12	95	TUCSON W/5T RESO	99	
X		144	94	ţ	85	1414 T/F-8A,O,+8B,O ATLANTA PN EQUALIZE	99	27
	4	160	103	10	85 85	14 4 SMEAR VS SCAN BALTIMORE WASHINGTON	99 99	93
		176	114	1 3A	75 75	1414 T/F+16,+8,0,-8,0 NEW YORK 1414 SMEAR SLITS PHILADELPHIA	95 95	121
		184	115			PN EQUALIZATION		
		225	130		80	1414 T/F+16,+8,0,-8,-16 DETROIT	99	34
		225	131			PROTECTIVE WRAP	e: "	108
						1208-1 FOOTAGE		1055
						ACCUMULATED FOOTAGE		

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	3.5	Missio	n 1208-2 S	pecial E	Events			
		REV	OPN .	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
		226				TRANSFER TO TU2-PREP I		
		227				COMPLETE TRANSFER-PREP 2		63
		248	139/141			PN EQUALIZE		
Appro		281	156			PBF A SET TO 76 PER PFA DIRECTION		
ved for R		291				IT-B SET TO -5 STEPS PER PFA DIRECTION		
elease		313	165/166			PN EQUALIZE		
高度数 単数単 ・		338	175	12	70	QUALITY VARIABILITY MIAMI	75	38
6/18 C		356	187			PN EQUALIZE		
0513		428	224			PN EQUALIZE		
7282		435	228	10 3A	70 70	1414 SMEAR VS SCAN NEW YORK 1414 SMEAR SLITS PHILADELPHIA	80 30	144
		451	234	3 A	70 70	1414 SMEAR SLITS BOSTON PROVIDENCE	99 90	49
		480				LEAK RATE TEST-5 SEC		
		493	254/256		,	PN EQUALIZE		

1757

*		REV	OPN	TEST	PRE	EVENT/LOCATION		VER	FTG
		496			WX	LEAK RATE TEST-180 SEC		WΧ	
		548	302	10	65 65	1414 SMEAR VS SCAN BOSTON PROVIDENCE	· ·	99 99	
		563				HPIVA OPEN			
		566	31)	3.1 7,9,12	95 95	1414 LENS MTF FLORENCE LINES TUCSON W/5T RESO		99 85	114
	4 5	629	338	,	75 75	1414 T/F+12,+6,0,-6,0 BOSTON PROVIDENCE		99 99	46
		631	339	10	75	1414 SMEAR VS SCAN LOS ANGELES		85	88
		647	346	6.1	95	1414 LENS MTF LUKE LINES		99	52
.*		A				1208-2 FOOTAGE			702
						ACCUMULATED FOOTAGE			

	3.6	Missi	on 1208-3	Special	Events	La companya da la co		
enzania de la constanta de la		REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
de y Caleb de Americanismo		678				TRANSFER TO TU3-PREP 1		
		679				COMPLETE TRANSFER-PREP 2		63
Approved		696	372	12	90	QUALITY VARIABILITY SACRAMENTO/ BAY AREA	80	30
Approved for Release: 2025/06/18 C05137282		728	388	6.2	95	1414 LENS MTF KINGMAN LINES 1414 LENS MTF	99	
se: 20					95	QUARTZSITE LINES	85	78
)25/06	43	744	397	7,9,12	90	TUCSON W/5T RESO	99	29
)/18 C051		752				XT-A SET TO +2 STEPS PER PFA DIRECTION		
137282		888	456	10	75	1414 SMEAR VS SCAN MONO B@-37° NEW YORK	85	83
	•	989	491			ESD A/B INDICATION		
		989 989				MONO À CV MONO B CV		12
		991				MONO A CV VIA DIS		12

	3.6	Missio	n 1208-3	Special	Events-(Cont'd.	And the same of th	
		REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
		993				SCC 2 SELECT MONO A CV VI A ENA		
		995				SCC HEALTH CHECK VI A DIS		163
•		1003	502	6.1	95	1414 LENS MTF FLORENCE LINES	95	50
2		1020				MONO A CV VIA ENA/DIS		12
		1092				PN EQUALIZE		
33		1099				SSP		
83						1208-3 FOOTAGE	•	437A 478B
						ACCUMULATED FOOTAGE		2144A 2235B

	3.7	Mission	1208-4 Sp	ectal E	vents			
		REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
		1115				TRANSFER TO TU4-PREP I		ı
		1116				COMPLETE TRANSFER-PREP 2		63
		1811	620	7,9,12	99	TUCSON W/5T RESO	99	29
		1268	641			PN EQUALIZE ESD B		
100		1277				PN EQUALIZE		
		1279				CREEP B		
		1283				CREEP B	2	*
-1-1		1287				DITHER TEST		
		1295				CV A-RELEASED FOR MONO A OPN JOG B	7	64
		1299				CREEP B		7

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	3.7	Mission	1208-4 Sp	ecial E	vents-Co	<u>n+†d</u> .			
		REV	OPN	TEST	PRE WX	EVENT/LOCATION		VER WX	FTG
		1300				SS ENGINEERING RELEASED FOR STEREO OPN	A		66
Approved for Release: 2025/06/18 C05137282		1309	651	-3A	75 75	1414 SMEAR SLITS -16,-8 BALTIMORE WASHINGTON		99 99	37
r Rele		1461				PN EQUALIZE			
ase: 2025/0		1487	719	.3A	65	1414 SMEAR SLITS -16,-8,0 NEW YORK		65	43
6/18 (1501				TRANSFER TO SO255			
205137		1528				PN EQUALIZE			
7282		1554	733	4,12	99	SO255 COLOR W/6C		99	37
		1570	741	8	95 95	S0255 COLOR W/6C VAN NUYS S0255 T/F 14,0,-14 LOS ANGELES		99	87
		1585	745	4,8	95	SO255 COLOR W/6C T/F +14 ST LOUIS		95	81

3.7	Mission	1208-4	Special	Events-Cont'd.

REV	OPN	TEST	PRE WX	EVENT/LOCATION	VER WX	FTG
1596				TRANSFER TO FE3916		
1633	756	3C	75	FE3916 SMEAR SLITS PHILADELPHIA	95	31
1635	758	5-	99	FE3916 W/6C STOCKTON	99	29
1651				PN EQUALIZE		
1656				PN EQUALIZE		
1667	764	5	65	FE3916 W/6C TUCSON	95	29
1687				PN EQUALIZE		
1700				PREP 2/CV		DEPLETED
•				1208-4 FOOTAGE		596A 605B
		1		ACCUMULATED FOOTAGE		2740A 2840B



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3.8

Solo Phase

No solo phase experiments were performed on mission 1208.

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4.0 SENSOR SYSTEM TEST OBJECTIVES

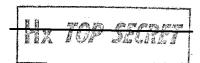
4.1 Photographic Performance

Determine the capability of the SS Optical System to provide the specified photographic performance.

The post flight material evaluation of mission segments 1208-1, 1208-2, 1208-3 and 1208-4 indicated in a general sense the capability of the SS Optical System to provide the specified photographic performance. Mission 1208 was a summer mission launched in April in a non sun synchrous orbit of 94.5° inclination angle, prior to the summer solstice. Summer missions in general acquire a large percentage of photography at solar altitudes above 30 degrees, resulting in smaller operational slits, shorter exposure times and less image smear. The overall image quality, however, was affected to some extent, as it always is at this time of the year, by varying degrees of weather and haze. In addition, specular reflections and shadowless acquisitions resulted in significant image quality degradations to the mission photography, similiar to Mission 1206.

In review, Mission 1206 was launched in July early in the afternoon in a sun synchronous orbit of 96.2 degrees following the summer solstice. This resulted in the specular reflection/front lighting problem to move south in latitude as a function of mission length, and the Jate launch caused the problem to locate at Nadir and simultaneously affect the imagery from both cameras. The sun synchrous inclination angle caused the problem to remain fixed in scan.

Mission 1208, however, was launched in April, early in the afternoon, prior to the summer solstice, at 94.5° inclination angle, non sun synchronous. This caused the specular reflection/front lighting problem to first move north and then slightly south in latitude. The lower inclination angle increased the precession and moved the local sun time over target closer to morning as the mission progressed. The problem, initially occurring near Nadir, moved across scan, as a function of mission length, ending up at approximately 30-35 degrees of scan at the end of the mission. Thus both cameras did not experience either anomaly at the same scan position.



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A much better operational plan for summer launches would be to launch early in the morning in a sun synchronous orbit. This places the anomaly out in scan, and the sun synchronous orbit fixes its position in scan. This intentional placement of the anomaly out in scan presupposes that operational target acquisition planning will not locate a large percentage of targets at these scan positions. Launching after the summer solstice will move the anomaly south away from the area of interest.

The general overall range in mission image quality for both cameras was very good to poor with the majority rated as fair to good. Orbital performance prediction using CRYSPER and the actual operational parameters are included in Figures 4-1 thru 4-4 for each mission segment and Figure 4-5 for the total mission length. A brief discussion of image quality and general photographic system performance as a function of mission progression is provided, abstracted in part from the PFA Rebound 831 messages.

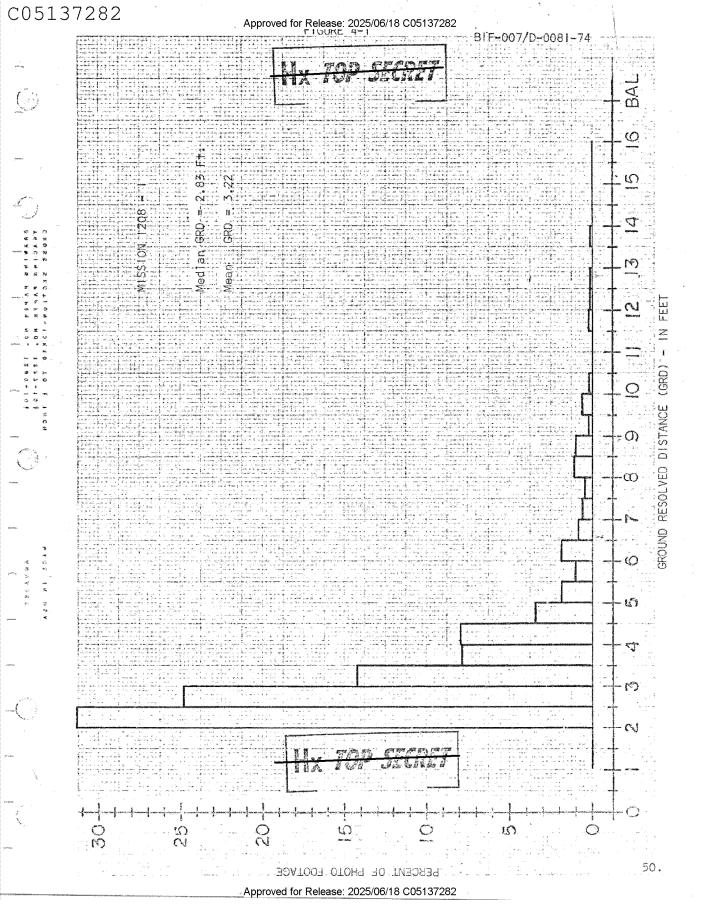
4.1.1 Mission Segment 1208-1

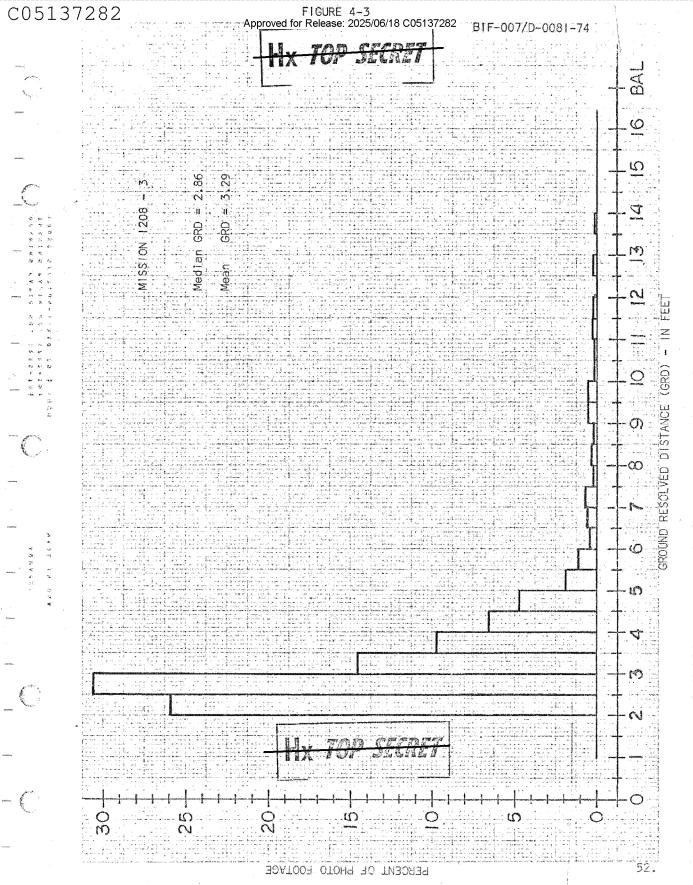
The overall image quality of both cameras ranged from very good to poor with the majority rated as fair. Analysis of the thru focus engineering ops both subjectively and with VEM, resulted in the PFA directing an eight micron retreat to the fwd camera platen, which changed the nominal platen to 76 microns. No focus change was made to the aft camera. In addition to the focus change on the fwd camera, an O2A2 change was required on the aft camera in-track of minus three command steps, resulting in a new in-track nominal setting of minus five command steps. No O2A2 adjustment was made to the fwd camera.

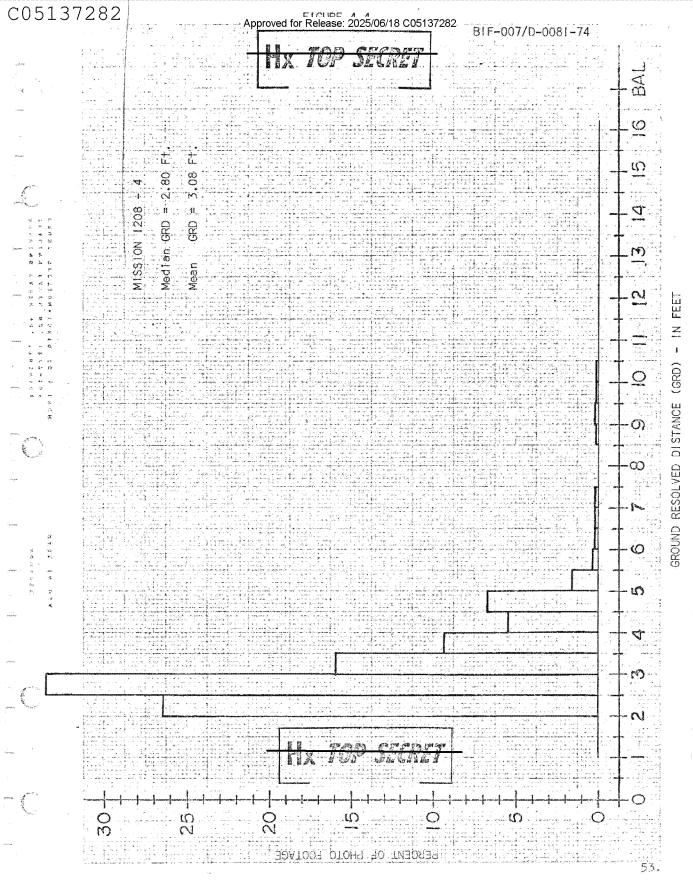
Subjectively, the image quality of the aft camera appeared to be sharper than that of the fwd. In point of fact, the very good imagery on this mission segment, was limited to clear weather acquisitions on the aft camera. The poor image quality which subjectively exhibited an overall grainy appearance, and soft unsharp edges was in part the result of non optimum acquisition conditions, such as high scan angles, cloud cover, medium to heavy haze levels, and the defocused condition of the fwd camera. The very good imagery from the aft camera was comparable to the better photography produced from past Hexagon Missions. This assessment was substantiated by the good resolution readings obtained from the tri-bar corn target, and the direct subjective comparison of image quality from previous Hexagon Missions.

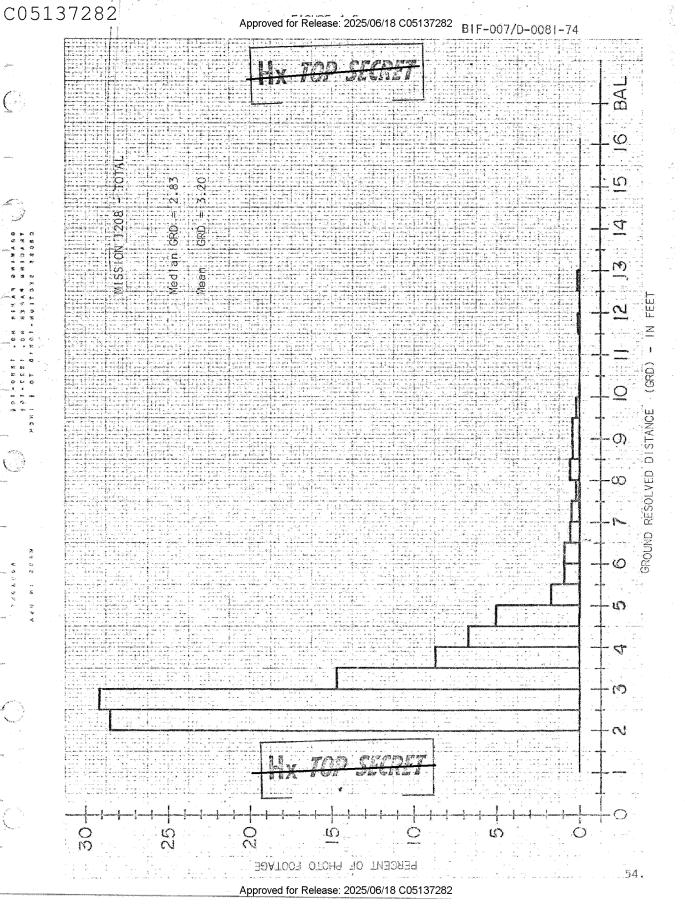
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One 51/51 tri-bar corn target was acquired on both the fwd and aft cameras. The data follows:

			ANG	LES		UNAL GRD.		2:1 GRD	ADJ (FT)
CAMERA	OP.	FRAME	SCAN	FIELD	PLATEN	IT	XT	IT	XT
fwd aft	084 084	004 004	+1.1	-0.8 -2.0	68 25		2.05 2.25	2.06 1.86	2.44 2.73

Exposure on this mission was based on a mean urban/industrial scene density of 1.10 instead of 1.00.

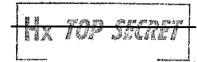
Microdensitometer analysis of 13 frames (9 fwd, 4 aft) with vegetation surround indicated reasonably good exposure (-.02 log E from aim for the fwd, -.05 log E for the aft) requiring no alteration of the 1208 general recommendation. The two count exposure reduction bias given to the aft camera resulted in a better balance exposure between cameras.

The average scene range was found to be higher than was generally recorded for this time of the year. This was true for both foreign and domestic ops. As was generally the case, the scene range of the domestic areas was greater as was the areas acquired by the fwd unit.

Although two snow scenes examined were correctly exposed, portions of two other frames were underexposed (op 58, frame 15 fwd, op 118, frame 17 fwd). In both frames urban areas were grossly underexposed with accompanying low contrast. Evaluation indicated that the snow had melted in the urban areas, and because the urban area represents only a small portion of the frame, the snow bias was correctly applied.

4.1.2 Mission Segment 1208-2

The overall image quality of both cameras improved on 1208-2 from 1208-1. This general improvement was attributed in part to the focus adjustment of plus 8 microns on the fwd camera, and in part to the overall improved atmospherics, resulting from less snow and correspondingly less moisture in the atmosphere. A third contributing factor was the use of the 26DN process employ—on 1208-2 because of abnormally high base plus fog on—ffic sections of both original photographic recor



4.1.2 Mission Segment 1208-2-Contid.

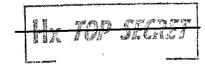
The image quality of both cameras on 1208-2 ranged from very good to poor with the majority rated as fair to good. As with Mission 1208-1, the very good imagery was associated with the aft camera. The aft camera image quality was superior to that of the fwd camera and subjective comparisons very clearly indicate that it was significantly sharper, and the aft camera consistently recorded very fine details. The fwd camera imagery was affected by specular reflections.

One 51/51 tri-bar corn target was acquired on both cameras. The data follows:

		, v	ANGI	LES		UNA GRD	DJ (FT)	2:1 GRD	ADJ (FT)
CAMERA	0P	FR	SCAN	FIELD	·	IT	XT	<u>IT</u>	XT
fwd aft	311 311	12 12	+16 +17	-1.7 -1.5	76 25	1.83	2.38 2.19	2.03 2.05	2.63 2.49

The late launch time of 1208 resulted in specular reflections on the fwd record, and full front lighting (shadowless acquisitions) on the aft photography. This condition occured near Nadir, and between approximately 5 to 30 degrees north latitude on this mission segment. This mission orbit was such that the specular reflections moved out in scan angle as the mission progressed and they were predicted to be at about 35 degrees scan at mission termination. The latitudes affected progressed to the north and then moved slightly south.

Many cases of specular reflections were found in the fwd camera imagery within the latitude bands and scan angles indicated. In this mission segment the effect of the specular reflections appeared more severe than the corresponding shadowless acquisitions. These shadowless acquisitions did in fact produce a loss in contrast due to the reduction of shadows in the scene, and a corresponding reduction in fine detail. The specular reflections occurred where ground water was standing. In these areas there was gross image blooming and loss of localized information in the direct vicinity of these reflections.



4.1.2 Mission Segment 1208-2-Contid.

A high base plus fog condition occurred on approximately 54 percent of the original negative. This condition existed on 1208-1 and was expected to be present throughout the remainder of the mission.

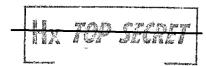
This anomaly was associated with specific manufactured film rolls and the probable cause was a pelloid backing contaminant, which, when in contact with the emulsion, caused a fog build-up with time, reduction of the density range, and a small speed and contrast change.

In an effort to compensate for the sensitometric change induced by the high fog found on 1208-1, EK evaluated several modified 19 DN processes. One of these, designated 26 DN, was selected for use on those segments of 1208-2 that could be expected to exhibit high fog in the standard 19 DN process. The 26 DN process reduced the fog somewhat and retained the desired sensitometry. Flashed stock was inserted at those manufacturing splices where a change from 19 DN to 26 DN or vise versa was required.

The developer switch was then accomplished as these flashed stock inserts were being processed and imagery was not affected by the transitions.

Comparisons were made of the duplicate positives from the normally processed low fog film, the 26 DN processed fogged film, and normally processed fogged film from 1208-1. The slightly increased contrast and the lower fog density of the 26 DN processed film over the 1208-1 fogged film was evident. More shadow and highlight detail was present in the imagery. Little discernable difference in image quality was present in comparisons made between the 26 DN processed fogged film and the normally processed low fog film in 1208-2.

Microdensitometer analysis of 29 acquisitions of vegetation surround, urban/industrial area imagery indicated generally satisfactory exposure with either 19 DN or 26 DN processing. The 26 DN process demonstrated higher contrast of the scene imagery accompanied by a slighter higher exposure of the scene mean (.02 log E). The high base fog level did not adversely affect any vegatation surround scene examined.



4.1.2 Mission Segment 1208-2-Cont'd.

Reported Snow Depth

Continued monitoring of springtime snow surround imagery indicated increased occurance of underexposed and flat imagery of cultured areas due to melted and/or dirty snow within the area of interest. Examples of this appeared in ops 307 and 308 where underexposure ranged up to a stop.

Because of the magnitude and frequency of underexposure of snow surround scenes, the following snow bias criteria was recommended for the remainder of the mission:

Exposure Blas

Less than 2 inches
2 to 10 inches
Greater than 10 inches
-.26 log E

While this change did not totally optimize exposure of snow surround scenes it was designed to prevent complete loss of information in shadow areas without grossly overexposing areas of existing snow.

4.1.3 Mission Segment 1208-3

The overall image quality of both cameras ranged from poor to very good. This imagery was comparable to 1208-2. The instances of poor photography was attributed to atmospheric conditions, very high sun angles, specular reflections, and shadowless imagery. The aft camera image quality was superior to that of the forward and most of the very good imagery was on the aft record. The presence of specular reflections and shadowless acquisitions, particularly front lighting, continued to significantly degrade a large portion of the photography from this mission.

These problems, particularly that of the front lighting, became more severe during this mission segment, with approximately 40 percent of the frames affected by front lighting. The most severe front lighting was similar to that seen on 1206. The problem was primarily due to the present sun/orbit geometry and large number of acquisitions in the latitude range from approximately 10 to 50 degrees north. Objects acquired between minus 10 and minus 20 degrees scan at these latitudes were degraded by front lighting, and objects acquired between plus 10 and plus 20 degrees were affected by specular reflections.

4.1.3 Mission Segment 1208-3-Cont'd.

For acquisitions within this latitude range north of the sub-solar point the aft camera was affected by front lighting, and the fwd camera experienced specular reflections. The effects appeared on opposite cameras in acquisitions south of the sub-solar point.

The magnitude of the degradation resulting from front lighting was dependent upon the camera to target to sun acquisition angle (cats angle). The extent of area affected ranged from a few degrees to as much as 20 degrees of scan in the most severe cases. The image degradation from the front lighting was more extensive than that from the specular reflections. All targets acquired with front lighting exhibited some degree of degradation, whereas specular reflections tended to degrade only high reflectance objects and their surroundings.

One 51/51 tri-bar corn target was acquired on both the fwd and aft cameras. The data follows:

			ΑN	IGLES		UNA GRD.	DJ (FT)	2:1 GRD.	ADJ (FT)
CAMERA	0P	FRAME	SCAN		PLATEN	IT	XT	IT	XT
fwd aft	397 397	3 3	- -	-1.5 -1.3	76 25	1.7	2.5	1.9	2.8

Microdensitometer analysis of vegetation surround urban area imagery indicated continued good exposure. There was also no significant change in mean scene density between use of 19 DN and 26 DN process chemistry. The following table gives the average exposure error of all vegetation surround scenes analyzed on 1208 (approx. 35 scenes) based on the optimum exposure criteria of 1.1 density.

AVG. MEASURED LOG EXPOSURE ERROR

		19 DN	26 DN
camera camera	×	minus .02 minus .04	minus .03



4.1.4 Mission Segment 1208-4

This mission segment contained 2588 feet of SO-255 conventional color material, and 3036 feet of FE-3916 infrared color material in addition to the regular 1414 black and white material. The photographic performance for each material type is as follows:

Film Type 1414 - Black and White The overall image quality of 1208-4 ranged from good to poor with the majority rated as fair to good. The instances of poor photography again were attributed in part to localized atmospheric conditions and specular/ shadowless acquisitions. As with earlier mission segments the majority of the good imagery was associated with the aft camera. The aft camera image quality was superior to that of the fwd in that it was sharper. The combination of haze and shadowless acquisitions resulted in poor imagery which can be characterized as flat and grainy. This yielded imagery with soft and unsharp edges and significant loss in fine detail. This condition had a lesser impact on total performance than on 1208-3.

Five 51/51 tri-bar corn targets were acquired on the fwd camera and one target on the aft camera. The data follows:

			ANG	LES		UNAI GRD.		2:1 / GRD.	
CAMERA	OP	FRAME			PLATEN	IT	XT	ĪT	XT
fwd	620	3	+21.0	+1.9	76	2,25	3.27	2.72	3.99
aft	620	4	+22.0	+0.1	25	2.10			2,68
fwd	741	4	-16.0	-0.3	76	1.72	1.95	2.58	2.89
fwd	745	3	- 8.0	-2.3	76	1.85	2.25	2.24	2.80
fwd	758	3	-27.5	-2.5	76	2,20	3.04	3.25	4.37
fwd	764	3	+14.0	0.0	76	1.78	2.66	2.24	2.80

Film Type SO-255 - Conventional Color

The quality of the imagery (for color film) ranged from very good to poor, with mose rated good. The very good imagery auality SQ-255 acquired with the was comparable to the Poor imagery was generally Hexagon System to data ints of haze. The color balance associated with large of the original was si tly yellow-green, and was similar to that of the SO-255 enquired on Mission 1207-1. Subjective evaluation of engineering photography for focus evaluation showed the nominal focus setting to be acceptable, although a slight bias to the plus side(6 microns) might have been in order.

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4.1.4 Mission Segment 1208-4-Cont'd.

Subjective evaluation of exposure showed the original to be slightly overexposed.

Two 51/51 corn tri-bar targets were acquired on SO-255 film. The data follows:

ÄNGLES						GRD.(FT)		
CAMERA	OP	FRAME	SCAN	FIELD	PLATEN	<u>IT</u>	XT	
aft	741 745	4	-15.3 - 8.0	-2.3 -0.5	55 55	2.83	3.03	

NOTE: Procedures for the 2:1 contrast adjustment have not been established for SO-255.

Film Type FE-3916 - (Infrared color)

The overall image quality of the FE-3916 material was good, and was comparable to that of 1207-4. The fine detail quality of the 3916, however, continues to be significantly less than that of the conventional black and white 1414 material utilized on the fwd camera. The color balance of the original has a slight cyan cast; subjective evaluation of the photography showed the exposure to be adequate.

Two 51/51 tri-bar corn targets were acquired on the aft camera on the FE-3916 material. The data follows:

			ANGLES						
CAMERA	OP	FRAME	SCAN	FIELD	PLATEN	IT	XT		
aft aft	758 764	3 4	-27.5 +15.0	-2.5 -2.3	55 55	5.66 4.80	6.21 5.94		

NOTE: Procedures for the 2:1 contrast adjustment have not been established for FE-3916.

The presence of specular reflections and shadowless acquisitions, particularly front lighting, continued to degrade portions of the photography from this mission segment.

The extent of the degradation within a frame (slight to severe) was approximately plus and minus 10 degrees of scan about the minimum cats angle with the most severe cases occurring between minus 20 and minus 30 degrees of scan at a latitude range of 40 to 45 degrees north for this mission segment.

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4.1.4 Mission Segment 1208-4-Cont'd.

Microdensitometer analysis of six SO-255 urban area acquisitions indicated an overexposure of approximately 0.10 log E. This overexposure was due in part to the overall scene brightness increase inherent in low shadow acquisitions. Low shadow scenes appeared quite frequently in aft camera acquisitions. This condition also appeared regularly in Mission 1206 with the same results in exposure. This amount of overexposure was considered significant and may have to be considered in the predictions of future summer missions.

Evaluation of three FE-3916 acquisitions showed a 0.08 log E overexposure. This was probably due in part to the shadowless conditions as well.

Although no microsensitometry was done on 1414 film in 1208-4 observation of clear weather imagery subjectively indicated continuing good exposure.

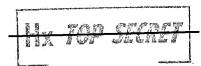
4.2 Take-Up Survival Thru Recovery

All the RV/TU assemblies arrived at the BRIDGEHEAD processing facility in good condition, with 1208-1 being a water recovery, and 1208-2,3 and 4 conventional air recoveries. The ability to maintain light tight integrity during orbital operations, separation, re-entry, recovery and transportation to the processing site, was fully demonstrated. The core locking pins were engaged and intact in TU's 1208-1,2 and 4 with the film well centered and stacked. The fwd camera core locking pin of TU 1208-3 was engaged and sheared and approximately 50 feet of film was spilled; on the aft camera, the core locking pin was engaged and bent causing some damage to the RV during pin removal. The film was well centered and stacked on both TU's of 1208-3. Small amounts of particulates were found in all the RV canisters.

Related de-filming observations for each mission segment follows:

4.2.1 Mission Segment 1208-1

The RV/TU arrived at the processing facility in good condition. All parachute apparatus was wet. The RV cover recesses had small amounts of water in them resulting from the wet recovery. The battery discharge units had not been installed on the RV. Both core locking pins were engaged and intact.



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4.2.1 Mission Segment 1208-1-Conttd.

Both film rolls were dry, well stacked and well centered in the T/U. A small amount of particulate was collected from the inside of the dome, as well as a one-inch long piece of wire which had been lodged in the fwd roll at OP 038 and had punctured four convolutions of the film. A severe dimple was detected near the head of the fwd roll at presplice. The cause was not found, but correlated with the puncture of fwd OP 001 IOR. Tag ends were removed and processed prior to normal defilming to allow early PFA team image quality evaluation.

4.2.2 Mission Segment 1208-2

The RV/TU arrived at the processing facility in good condition. Both core locking pins were engaged and intact. Both rolls were well stacked and well centered on the TU with no festooning into the dome. The hinge and thermal access door on the entrance side was sprung. A white residue was noted around the fwd side exit door and cutter assembly.

During despooling it was discovered that the brake on the fwd side was not operational. It was commanded "on" several times but no braking could be accomplished. The audible sound of the brake solenoid actuation was detected thus concluding the problem to be in the brake assembly. This necessitated hand held tension on the stack when the motor was turned off for splicing.

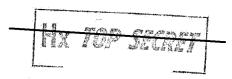
Two deep scratches were noted inside the dome and a I inch tear in the acrylic tape covering the fiberglass on the relay housing was noted on the fwd side adjacent to a canister alighment pin.

The dome was clean with only a small amount of particulate retrieved.

4.2.3 Mission Segment 1208-3

The RV/TU arrived at the processing facility in good condition.

Upon removal of the RV canister, it was evident that the de-orbit core locking pin on the fwd side had sheared resulting in a 50 foot film spill. Prior to handling the film, the builder roller arms were raised



63.

4.2.3 Mission Segment 1208-3-Cont'd.

electrically using special test equipment. This was to preclude possible damage to the builder roller verify microswitch on the fwd side which evidenced intermittent failure during the mission. The 50 feet of spilled film was then responded onto the TU stack.

The film stacks were good with the exception of a rough edge on the inside of the fwd stack approximately 3/4 inch from the outside diameter.

The most significant problem occurred when attempting to withdraw the aft core locking pin that had been bent during recovery. Normal techniques for removing a bent pin failed, requiring the pin assembly to be drilled out. This effort consumed 18 hours. However, processing time was not lost because the fwd side film was processed in parallel with this effort.

The RV suffered the following damage during removal of the bent core locking pin:

- 1. Complete destruction of the piston and actuating pin.
- 2. Cut wire bundle and damage to the solenoid assembly.
- 3. Removal and damage to actuator assembly plate.
- 4. A fracture in the support assembly cross frame member of approximately 7mm.
- 5. Damage to primary battery.
- 6. Minor physical damage (rubs, abrasions, etc.) to the aft side wire bundles in area of A-2 canister recess.

A small amount of particulate was retrieved from the dome.

4.2.4 Mission Segment 1208-4

The RV/TU arrived at the processing facility in good condition. No major problems occurred. The film stacks were good and the de-orbit pins did not shear. A small amount of shredded film was found in the RV cannister. The film was damaged by pulling the loose ends thru the camera. The TU electronics (A-2 and A-15) on aff side were removed and sent directly to the vendor for analysis of the integrator reset problem experienced during 1208-4 mission segment.



4.3 Optimum Focus Determination

Mission 1208 (SV8/SN11) was launched with orbital focal plane settings of 68 microns on the forward camera and 25 microns on the aft camera. These settings included a plus 14 micron adjustment on both cameras for the altitude shift from infinity (A-2 collimator settings) to 85 nautical miles mission altitude. They also included a minus 15 micron adjustment on the forward camera and a minus 19 microns on the aft camera for the folding flat gravity effects. The forward camera was further adjusted plus 2 microns to account for a defocus of the test collimator.

Following the evaluation of the on orbit thru-focus tests in RV-I a retreat of plus 8 microns was recommended for the forward camera. The forward platen was retreated to 76 microns on OP 156. No focus change was deemed necessary for the aft camera.

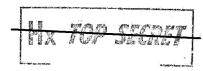
A change in focus of plus 30 microns retreat was implemented on the aft camera when the material switched from 1414 black and white to the SO-255 conventional color. This focal plane position was also utilized for the FE-3916 infrared color material.

4.4 Optimum OOAA Settings

On-Orbit smear data was collected during all four of the mission segments of Mission 1208, on either the 1414 material or on the FE-3916 infrared color. No smear data was collected on the SO-255 conventional color material.

Analysis of the smear test material from mission segment 1208-1 identified an aft camera in-track velocity error. It was determined that the film velocity was 0.023 ips too fast and the PFA directed a minus three command step change to correct it. The ground settings for the forward camera, in-track and cross-track and the aft camera cross-track were determined to be correct. It is interesting to note that since the first use of smear slits on SV-6, all three systems have required an identical change to the aft camera in-track settings. This phenomenon is currently under investigation.

On mission segment 1208-2 ninety data points were measured from each camera. The minus three command step change made to the aft camera in the in-track direction was verified to be correct and within less than one command step of the indicated



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4.4 Optimum OOAA Settings-Cont'd.

zero setting. The forward camera in the cross-track direction showed that the indicated mean error was slightly greater than one command step and was changed accordingly by plus one command step. The forward camera in-track and aft camera cross-track directions were both confirmed to be properly set. The smear slit imagery, both subjectively and objectively, indicated higher smear variability then past systems. Only one smear test (a type 10) was run on mission segment 1208-3, and this was a mono run on the aft camera. This data was not reduced.

Mission segment 1208-4 contained 2588 feet of SO-255 color and 3036 feet of FE-3916 infrared color material included in the aft camera record. No OOAA tests were acquired on the SO-255 material, however, subjective evaluation of the smear slit imagery indicated that the cross-track bias was adequate to account for the difference in material thickness.

A subjective evaluation of the smear slit imagery acquired on the FE-3916 material was performed. The inherent low resolution level of the IR film and subsequent very poor image quality in the smear slits negated any quantitave measurement or subjective assessment of the cross-track film synchronization. The PFA recommended that this test on FE-3916 not be performed on subsequent missions. Special thru-focus/0²A² bias tests were conducted during this mission segment to determine if the minus eight microns focal plane bias was optimum. Analysis of the material indicated that the bias magnitude and direction was necessary and adequate.

4.5 Optics Thermal Profile

The following subparagraphs describe the thermal environment for Mission 1208. Definitions of measured and calculated temperature parameters are contained in the Mission 1207 Post Flight Report, PM-1496-X. Thermal control for SV-8 can be generally summarized as follows:

 All SS temperatures were within design limits throughout the mission.



4.5.1 SV Environment

SV thermal control parameters are summarized as follows:

* Orbital Elements (Ref. Paragraph 1.5)

Perigee Altitude

 $h_{p} = 85.6 \text{ n.m.}$

Period

 $\tau = 88.5 \, \text{min.}$

Inclination

 $I = 94.5 \deg.$

Argument of Perigee

 $\alpha = 130$ deg.

Beta

 $\beta = -2.6 \text{ deg. (Rev I)}$ $\beta = 26.5 \text{ deg. (Rev I692)}$

Midsection Thermal Control Design Values

Cocoon

 $\alpha/\epsilon = 0.359/0.265$

Thermal Baffle

 $\alpha/\epsilon = 0.90/0.90$

MLI Effective Emittance

Lower 210 Degrees

e* = 0.0045

Fwd & Aft Bulkheads

 $\epsilon * = 0.0045$

Viewport Baffle

e* = 0.0045

Under TCA Cocoon

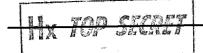
 $\varepsilon * = 0.04$

Under SU Cocoon

 ε * = 0.6

4.5.2 TCA Environment

Table 4-1 is a summary of temperature levels, spatial distributions, and temporal variations over a typical orbital revolution in terms of the thermal ICD (1420316A) requirements. Figures 4-6 thru 4-8 show the corresponding orbital profiles of the ICD parameters.

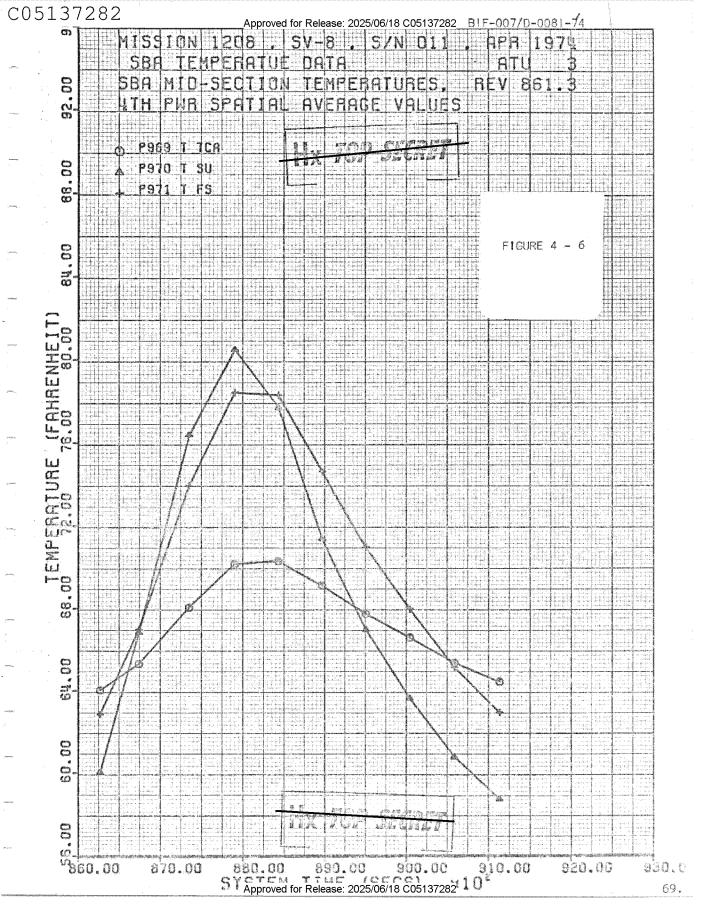


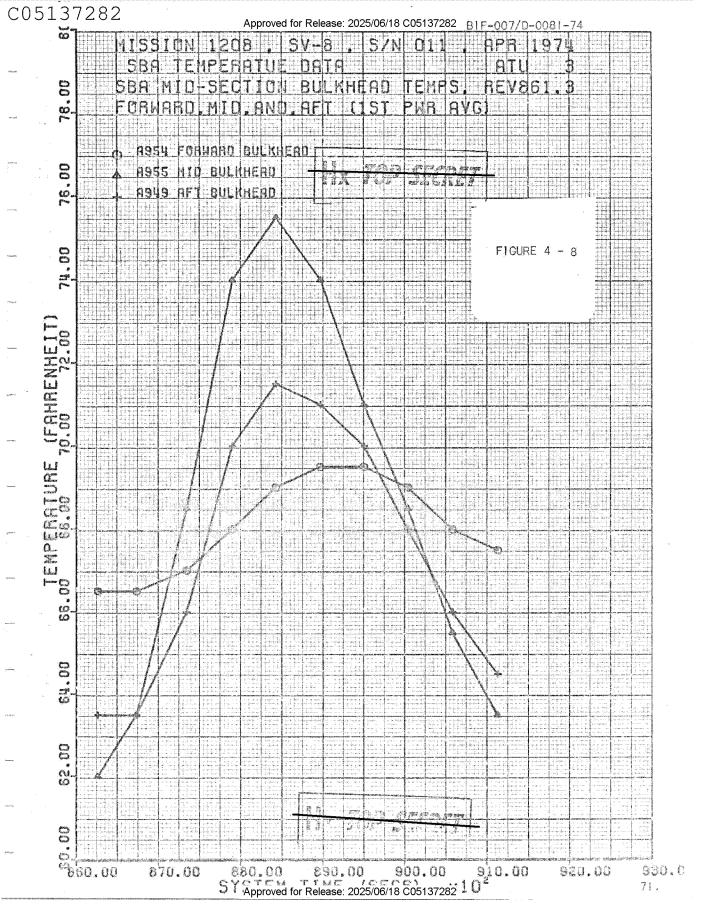
TCA COMPARTMENT TEMPERATURES

(MISSION 1208 REV 861)

in ton	Designated Zones	Max Allowable ICD Value(°f)	Flight Value(°f)
Temperature Level Index (T TCA) Zone I Mean Temp. Zone II Mean Temp. Zone III Mean Temp. Zone IV Mean Temp. Forward Bulkhead Middle Bulkhead	Not Applicable	70 ± 21 N/A N/A N/A N/A N/A N/A	67 65 66 69 68 69
Variation of Mean Temp. Between Designated Zones	l to IV II to III I to II III to IV Bulkhead to Bulkhead	9 6 4 4 6	2 2 3
Spatial Variation of Time-Average Temp. Measurements at Locations Within Designated Zone	 V Forward Bulkhead Middle Bulkhead	11 9 9 11 5 17	5 2 1 1 2 6
Temporal Variation (Peak to Valley) of Temperature Measurement at any one Location within Designated Zone	 	46 20 20 46 26 57	17 1 17 4







C05137282



4.5.3 Optical Bar Temperatures

Tref was 67 $^{\pm}$ 1°f throughout the mission. The equilibrium temperature levels for the A and B optical bars were approximately 66°f and 65°f respectively. Figure 4 - 9 shows an orbital profile of the OB temperatures in the stowed position.

73.

5.0 SCF SUPPORT

5.1 'TUNITY 'Mission 1208

The 'TUNITY MOD-2 software for Mission 1208 performed all of its functions nominally except for the following software problems.

In message 350, Rev 123, Operation 3, a desert polygon bias was applied where no desert polygon had been defined. This caused the operation to be under-exposed. A change was made to 'TAPWRP correcting the problem. The change was incorporated on the Flight Auxiliary Master.

Check message 38 appeared often, flagging insufficient time between FT- and C-. Errors flagged ranged up to .289 seconds. This problem occurred by tightening check message 38. The problem was determined to be flight critical because message 38 was in error due to truncation in both 'TFUNCHK and 'TUMP. Changes were made to both 'TFUNCHK and 'TUMP correcting the problem. The change was incorporated on the Flight Auxiliary Master.

5.2 Augie

5.2.1 Overall Performance

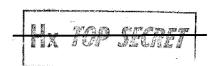
Real time performance of Augie data met all requirements expected. SSC real time modes are limited to verification of SS status. Playback performance of Augie data met all requirements expected. Time delays for play backs of data was reasonable with few exceptions.

5.2.2 Modifications

No changes to the Augie modes were required during the flight. One MCR was required to correct the processing of the shutter open and close telemetry monitors, this was a deficiency in the handling of the data by the mode processing.

Mode Change Requests have been submitted to change or add telemetry data processing to the mode for the next flight. The MCR's submitted are for the following reasons:

a. Change processing of shutter open and close telemetry so as to calculate and output shutter open and close times to OB position in degrees.



5.2.2 Modifications-Cont'd.

- Correct Supply Command Signal processing to increase accuracy of output.
- Output slit width A & B telemetry data by using the change in DIU counter to clock out the next sample of slit width A & B telemetry data.
- d. Add Take-up Integrator Output telemetry monitors to the Format C diagnostic modes.

5.2.3 D.T.V.

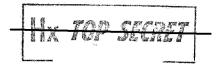
SSC utilization of the DTV was limited to passive real time SS status verification. The use of the DTV will remain limited to status monitoring on the next flight also.

5.3 RTS Tapes and Microwave

5.3.1 RTS Tapes

RTS tapes were used minimally during the last half of the flight due to use of the microwave link between the STC and Bldg. 156. The tapes that were utilized, the majority being COOK, met SSC requirements with few exceptions.

5.3.2 The microwave capability between the STC and Bldg. 156 did reduce the number of tapes required by SSC tremendously. The link did experience many problems during the first portion of the flight, most of the problems fell into the category of not having the proper procedures set-up, however, most of these problems were corrected during the flight. Continued use of the microwave link with the STC is planned for the next flight.

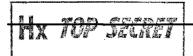


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APPENDIX

A-1

OPERATIONAL SUMMARY



1208-1

CAMERA OPERATIONS SUMMARY REVS PAD THROUGH REV 225, OP 131

EV	MSN CP	SCA	SCC	FRAN	4 E.S		ERCP	PHCT	C-FT	CUM-TU	-FEET
porter	NUM			FhC	AFT	FER FWC	AFT	FWD	8 E T	ė.	4 / T
RE	LC	6:C	0			7.2	78		AFI	FND	AFT
PRE	LC	60	0	6	6 6	35	34	33 33	3.3	105	111
-DRE	LO	3 C	30						3.3	173	178
			6. 27	6	6	76	69	1.7	17	266	264
>RE	LC	6.0	15		4	11	2.0	40	2.3	317	307
PRE	ra	3.0	30	6	6	3	11	17	17	337	335
PRE	LC	60	15	7	4	11	20	40	23	388	378
*RE	FC	120	C	8.	8	38	7.0	87	87	513	535
≯RE	LC	120	C	8	8	111	111	87	87	711	733
PRE	LC	60	0	ć	6	81	63	33	33	825	831
⊃RE	LC	6 C	C	6	6	31	31	33	33	889	895
2RE	LO	60	C	6	6	31	31	33	33	953	959
PRE	LC	3 C	3.0	ć	6	68	5.3	1.7	17	1038	1029
-DRE	LC	6 C	15	7	4	11	2.0	40	2.3	1089	1072
PRE	LC	6 C	C	6	6	8	163	3.3	3.3	1130	1268
PRE	LC	3 C	3.0	6	6.	26	18	17	17	1173	1303
PRE	LO	6 C	15	7	4	11	20	40	23	1224	1346
>8 E	LO	12C	Ç	8	8	38	7 C	87	87	1349	1503
>RE	ŁC	120	0	8	8	111	111	87	87	1547	1701
PRE	LO	6 Ç	C	6	6	81	65	3.3	33	1661	1799
TORE	LO	60	0	6	6	31	Эì	33	3.3	1725	1863
PRE	LC	6 C	C	6	6	31	31	33	33	1789	1927
PRE	LC	6 C	C.	6	6	31	31	33	3.3	1853	1991
- 4	1	60	0	6	6	126	126	33	3.3	2C12	2150
4	2	6 C	-15	6	6	24	25	3.3	33	2069	2208
4	3	6 C	3 C	6	6	36	35	3.3	3/3	2138	2276
5	4	3.0	-30	50	50	3.0	24	145	145	2313	2445
6	5	6 C	O	31	31	2.2	30	171	173	2506	2646
7	6	90	O.	3 €	38	4.8	55	3¢8	308	2862	3009
7	7	3 C	0	7	7	49	2.3	25	2 C	2931	3062
8	8	6.0	e	6.	€.	19	28	33	3.3	2993	2123
. 8	9	6 C	3.0	16	16	36	34	8.8	8.8	31.07	3245
9	1 C	6 C	-15	16	16	35	37	98	8.8	3230	337C
- 10	1.1	90	G	6.8	68	46	5.3	551	55X	3827	3974
10	1.2	90	C	2:3.	2.3	67	67	186	186	4080	4227
14	23	3 C	0	14	14	49	33	40	4 C	4169	4300
16	14	3.0	Q.	5	5	14	14	14	15	4197	4329
19	15	3 C	3.0	7	7	14	13	20	2 C	4231	4362
21	16	3 C	-45	5.3	53	14	14	148	148	4393	4524
21	17	60	1.5	2.3	23	22	29	127	127	4541	4680
23	1.8	90	0	25	25	50	57	203	203	4794	4940
24	15	6.0	-30	23	23	5.5	4.8	127	127	4976	5115
25	20	3.0	-30	10	10	28	20	28	28	5032	5163
- 25	21	60	-15	8	8	20	28	44	44	5 C 9 6	5235

	£ 2	2.50		0.0	0.0	70.00	-	10.00	222	2023	2022
25	23	90	15	15	15	67	66	122	122	5882	6027
26	24	9.0	0	3.8	28	67	6.7	227	227	6176	6321
26	25	60	0	50	50	5.5	48	275	275	6506	6644
26	26	3.C	30	2.8	28	25	22	81	81	6616	6747
27	27	3 C	45	25	25	14	14	73	73	6703	6834
- 28	28	3 C	4.5	16	16	13	13	46	46	6762	6893
38	29	120	0	6.2	62	36	70	664	664	7462	7627
38	3.0	60	-30	36	36	79	64	198	198	7739	7889
- 38	31	6 C	.15	13	13	37	36	72	7.2	7848	7997
39	3.2	90	15	22	22	4,4	51	178	1.78	807C	8226
4)	33	6 C	-3C	35	35	52	46	193	193	8315	8465
41	34	9.0	0	108	108	5 C	57	875	875	9240	9397
41	35	6 C	15	18	18	57	49	99	99	9396	9545
41	36	3 C	30	2.8	28	3 C	22	81	81	95C7	9648
42	37	6.0	15	19	19	21	29	105	105	9633	9782
- 43	3.8	60	-30	26	26	34	36	143	143	9810	9961
4.8	39	6 C	-15	33	33	36	35	182	182	16	
- 53	40	3 C	-15	29	29	30	21	84	84		
										10142	10283
- 54	41	3.0	45	7	7	14	14	20	20	10176	10317
56	42	3 C	45	13	1.3	24	14	38	3.8	10228	10369
57	43		, C	89	89	3.2	48	720	72 C	10980	11137
57	44	3 C	0	5	5	49	33	15	15	11044	11185
5 €	45	90	-15	122	122	3 C	47	988	988	12062	12220
58	46	3 C	-30	7	7	49	33	20	2.0	12131	12273
59	47	60	15	31	31	21	28	171	171	12323	12472
- 68	48	3 C	c	4	4	29	21	12	1.2	12364	12505
7.0	49	60	15	22	22	22	29	121	121	12507	12655
71	50	120	0	35	35	64	81	375	375	12946	13111
73	51	90	15	65	65	91	83	527	527	13564	13721
76	52	90	0	16	16	68	68	130	130	13762	13919
8 C	53	90	0	37	37	67	67	300	300	14129	
81	54	3.0	C	14	14	50	35	41	41	14220	14362
86	55	60	-30	-50	2.0	22	31	110	110	14352	14503
27	56	6 C	-30	26	26	38	38	143	143	14533	14684
87	57	13C	C	68	68	67	ક 🏃	728	728	15328	15493
- 88	5,8	90	0	25	2.5	90	8.2	203	203	15621	15778
99	59	6 C	15	LC	10	57	48	55	55	15733	15881
89	6 C	3 C	30	26	26	25	22	75	75	15837	15978
89	67	9 C	0	26	26	33	50	211	211	16081	16239
9.0	62	60	-15	12	12	58	50	66	56	16205	16355
96	63	60	-30	8	8	37	37	44	44	16286	16436
97	64	60	30	16	16	37	3.5	88	88	16411	16559
TLG3	65	90	ō	86	86	45	54	697	697	17153	17310
104	66	6.0	-15	3.8	38	52	45	209	209	17414	17564
104		9.0	15	2.8				227	227	17684	17840
	6.7				28	43	49				
1.05	68	60	C	41	41	52	45	226	226	17962	18111
1.05	65	12C	0	35	35	62	78	375	375	18399	18564
106	7 C	3.0	- 30	6.5	65	71	4.8	189	189	18659	18801
1.06	71	6 C	30	34	34	21	28	187	187	18867	19016

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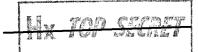
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201	122	3 C	C	10	10	74	51	29	29	26672	26814
202	123	6 C	0	46	46	21	29	253	253	26946	27095
-2C3	124	3 C	30	31	31	29	21	90	90	27065	27206 .
:16	125	3 C	3 C	14	14	14	14	41	41	27120	27261
216	126	120	0	3 č	36	51	75	385	385	27556	27721
216	127	60	15	19	19	82	65	105	105	27743	27891
218		3 C	15	4	4	29	22	12	12	27784	27925
218	129	6 C	C	22	22	22	3.0	121	121	27927	28076
225	13C	3 C	30	7	7	29	21	20	2 C	27976	28117
₹25	131	60	· C	4	2	21	3 C	22	15	28019	28162

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225	131	6 C	0	7	ç	0	0	43	51	43	51			***************************************	1
230	132	3.0	-3¢	4	4	85	81	12	12	144	144				
-232	133	6 C	15	3.1	31	2.2	29	171	171	337	344				
232	134	90	G	59	59	49	57	478	478	864	879				
239	135	3 (-15	6	6	49	33	17	17	930	929				
_235	136	60	C	-8	8	2 C	29	44	44	994	1002				
2.3 €	137	3 €	3 C	8	8	29	20	23	23	1046	1045				
247	138	120	C	26	26	38	62	278	278	1362	1385				
248	139	6 C	15	16	16	69	53	8.8	8.8	1519	1526				
724.8	140	30	-3.C	26	26	28	21	75	75	1622	1622			*	
248	141	9 C	-15	54	54	3.5	51	437	437	2094	2110				
249	142	-9€	C	19	15	69	68	154	154	2317	2332				
-250	143	60	15	31	31	54	46	171	171	2542	2549				
250	144	9 C	C	10	1.0	47	5.5	81	81	267C	2685				
25%	145	60	15	16	1.6	54	46	88	8.8	2812	2819				
251	146	6 C	15	44	44	37	3.7	242	242	3091	3098				
252	147	6 C	-15	8	8	34	35	44	44	3169	3177				
252	148	3 C	-15	16	16	27	19	46	46	2342	3242				
253	149	3 C	15	10	1 C	14	13	29	29	3285	3284				
~253	150	6 C	-15	23	23	20	29	127	127	3432	3440				
258	151	3 C	-15	6	6	30	22	17	1.7	3479	3479				
268	152	3 C	-30	23	23	14	13	67	67	3560	3559				
-268	153	3 C	-3C	14	14	14	15	41	. 41	3615	3615			*	
269	154	6 C	15	16	10	20	27	8.8	88	3723	3730				



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.338	176	3 C	15	8	8	14	13	23	23	8474	8473
43	177	3.0	-15	4	4	14	15	12	1.2	8500	8500 .
545	178	60	0	61	61	22	29	336	336	8858	8865
346	179	3 C	-15	16	16	29	22	46	46	8933	8933
46	180	3 C	3 C	13	13	14	13	. 38	3 €	8985	3984
47	181	3 C	-45	14	14	14	15	41	41	5 C4 C	9040
347	182	3 C	-45	17	17	14	14	49	49	9103	9103
748	183	3 C	C	25	25	14	14	73	73	9190	9190
-48	184	3 C	-30	9	9	14	14	26	26	9230	923C
349	185	6 C	C	32	32	22	29	176	176	9428	9435
_355	186	3.C	-30	14	14	29	22	41	41	9498	9498
156	187	3 C	30	11	11	15	13	3.2	32	9845	9543
359	188	3 C	45	4	4	14	14	12	1.2	9571	9569
361	189	6 C	-15	34	34	22	30	187	187	9780	9786
163	190	120	C	2.8	28	64	80	300	30C	10144	10166
:64	191	6 C	-3C	11	11	8 C	6.5	61	61	1C285	10292
365	192	3 C	-45	13	C	3.0	0	38	Ċ	10353	10292
365	193	30	С	6	6	14	21	17	17	10384	10330
17C	194	30	45	1 C	10	13	13	29	29	10426	10372
376	195	3 C	45	25	0	13	C	73	C	10512	10372
378	196	3.0	C	19	19	14	14	55	5.5	10581	10441
379	197	3 Ç	-15	ŝ	· · · · · ·	14	14	26	26	10621	10481
379	198	30	45	13	13	14	13	38	3.8	10673	10532
381	199	3·C	-30	4	1	14	15	12	12	10699	10559
381	200	3 C	30	43	43	14	13	125	125	10838	10697
382	201	3 C	45	7	7	14	14	21	21	10873	10732
383	2 C 2	30	45	7	7	15	15	21	21	10909	10768
-389	203	3.0	-30	4	4	14	15	12	12	10935	10795
394	204	90	0	28	č	27	Č	227	2 2	11189	10795
394	205	3 0	-15	4	4.	44	14	12	12	11245	10821
394	2.C.6	6 C	Ĉ	15	15	22	29	83	83	11350	10933
	207	60	15	35	35	35	35	193	193	11578	11161
396	208	90	-15	3 C	3 C	46	55	243	243	1,867	11459
396	209	30	3.0	11	11	48	31	32	3.2	11947	11522
396	210	30	-30	63	63	14	15	183	183	12144	11720
399	211	30	15	15	1.5	34	12	55	55	12213	11787
399	212		45	16	10	12	13	29	29	12254	11829
-410	213	3.C 3.C	-30	1.7	17		15		49		
					A. /	14		49	C	12317	11853
411	214	9 C	15	31		28	0 27	251		12596	11893
412 _412	215	60	15	29	29	50		160	160	12806	1208C
	216	60	-30	3.0	30	35	37	165	165	13006	12282
412	217	3 C	-15	23	23	30	21	67	6.7	13103	1237C

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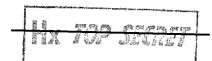
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			3		pry regs	20					3 C05137282	BIF-00)7/D-008	31-74
	274 275	S C.	C -45	27	27	3.5	51	219		18940			America Mariante America	
-	276	30	30	14	14	49	34	41		19030 19082			87 FD FD	gran raid
	277	3.0	30	14	14	14	13	38 41	3.8	19137		HX		DEG
	278	3 C	30	22	22	14	14					0 83.7	Mi Jensey	-
	275	30	-3C	18	18	14	14 15	64		19215	18223			
25	28C	30	3 C	# C		15	14	52	52					
526	281	3 ¢	30	4	8	14	14	23 12	23		18327 18353			
	282	60	C	19	15	22	3 C	105	105	19472				
-27	283	3 C	45	4	47	29	21	1.2	12		18521			
	284	3.0	-3C	10	10	14	15	30		19557				
	285	3 C	-15	14	14	14	14	41	41	19612	13621			
	286	30	45	7	7	14	13	20		19646				
32.8		90	ć	35	35	34	50	284		19964				
528	288	3.0	-30	21	21	49	33	61			19082			
	289	3 C	-30	4	4	14	14	12		26100				
	290		-3C	7	7	14	13	20		20134	19141	ŧ.		
	291		-15	16	16	14	14	46		20194			6.	
541	292		-15	35	35	20	28	193		20407				
	293		-15	25	25	29	20	73		20509				
42	254		-15	13	13	14	15	38		20561				
542	295		-15	14	14	14	14	41		20616				
	296		-15	7	7	13	13	20		20649				
543	297	90	Ć	3.5	35	29	44	284	284		19984			
	258	3.C	-45	3.2	32	44	29	93		21099				
	255	30	C	3.	8	14	13	23	23	21136				
	300		-3C	36	36	13	14	104		21253				
544	3C1	30	-30	15	15	14	14	44		21311				
548	302		-30	13	13	21	∠9	72		21404				
556	303	30	-15	ì.C	10	29	21	29	2.5	21462				
559	3C4	6.C	15	25	25	19	26	139		21619	20633			
555	305	3 C	-15	4	4	27	19	12		21658				
-559	306	30	-30	4	4	14	15	12		21684				
559	307	30	15	å	4	13	13	12	1.2	21709	20716			
560	308	30	0	13	13	14	12	38	38	21761	20757			
561	309	30	-45	Žć	26	13	14	73	7.5	21849				
Lòc	31 C	3 C	15	16	16	14	13	46	46	21909				
	311	6 C	15	14	14	22	30	77		22008				
572	312	30	-30	35	35	29	22	102		22139				
574	313	έC	-15	26	26	21	29	143		223C3	21318			
574	314	90	0	31	31	49	56	251	251	22603	21625			
575	325	6.0	15	34	34	56	47	167	187	22846				
_575	316	30	-30	1 C	ĩc	28	22	29		22903				
575	317	3.0	-30	4	4	14	14	12	12	22929				
575			-15	3.2	1.2	14	14	35		22978				
212	24.0	20	4.0	Se die	A CO	表""	7.77	برد	جدر کان سعاد	EE.710	E.B 9 G.A			

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29 23021 22027

72 23115 22129

77 23228 22242

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Approved for Release: 2025/06/18 C05137282

64 23500 22506

160 25709 24715

96 25819 24826

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PEPDES

178 23710 22732

593 326 6 C 138 23903 22917 103 327 -30 88 24C26 23O41 J04 328 3 C 99 24154 23160 -15 606 329 2.5 6 C 138 24314 23328 507 33C C 55 24406 23420 108 331 3 C 29 24464 23470 508 332 3 C 237 24723 23737 -15 -:22 333 138 24898 23913 123 334 105 25053 24075 381 25501 24523

625 335 £26 336 3 C :26 337 -30 029 338 -15 3.0 631 339 6.0 -30

34C 3 C 3 C 3 C -3C

-639 343 :41 6 C C -30 3 C 3 C C 553 347 -3C

-15 354 348 6 C 655 349 3 C 356 350 3Ċ 556 351

656 352 3.0 -557 353 -3C 157 354 669 355 3 C 669 356 6 C

:71 357 -45 3 C 271 358 -15 671 359 -15 3 C ő 372 360

572 361 3 C -30 1.0 673 362 Ċ -673 363 6 C 1.7 574 364 ς

32 25865 24872 5C 25937 24952 23 25590 24996 81 26085 25092 26134 25141 26198 25205 88 26306 25320 232 26565 25572 38 26617 25623

267CO 25715 8E 26825 2584C 2 C

26875 25881 72 26968 25982 15 27012 26018 15 27 042 26048 67 27122 16129

389 27543 26565 46 27637 26643 88 27747 26761 20 27796 26803 176 27994 27009

17 28041 27048 136 26201 27215 29 28259 27286 275 28567 27589

94 28717 27731 65 28846 27854

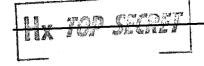
Approved for Release: 2025/06/18 C05137282

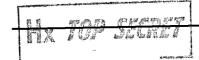
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В.

CAMERA OPERATIONS SUMMARY REV 674 CP 364 THROUGH REV 1111 OP 577

3EV	MSN CP	SCA	scc	FRAI	4 E S	INT	ERCP	PHOT	C-FT	CUM-TU	-FEET
series.			all the same of th	e	8 27 T			20.00		e 1 / 2	A POTE
	NUM			FWC	AFT	FWD	AFT	FWD	AFT	FhD	AFT
:74	364	90	0	2	3	C	0	11	26	11	26
685	365	90	C	37	37	13C	130	300	300	441	456
-686	366	3.0	730	13	1.3	49	33	38	38	528	5.27
18.6	367	3.C	3 C	11	11	14	13	32	32	574	572
687	368	3 C	-45	32	32	14	15	93	9:3	681	680
687	369	90	С	53	5.3	34	50	429	429	1144	1159
389	37C	3 C	45	7	7	49	31	20	2.0	1213	1210
389	371	6 C	C	17	17	21	3 C	94	94	1328	1334
696	372	30	0	18	18	25	21	52	5.2	1409	1407
-7C1	373	3 C	-3C	4	4	14	15	12	12	1435	1434
/C1	374	9 C	С	14	14	34	49	332	332	1801	1815
702	375	3 C	30	25	25	49	33	73	73	1923	1921
-7C4	376	30	30	7	7	14	14	20	2.0	1957	1955
764	377	3.0	30	16	16	14	14	46	46	2017	2015
705	378	6 C	-15	32	3.2	22	31	176	176	2215	2222
706	379	3 C	15	4	4	30	21	12	12	2257	2255
706	380	3.0	30	2 C	20	14	14	58	58	2329	2327
714	381	60	15	10	10	21	29	55	55	2405	2411
715	392	3.0	45	4	4	28	20	12	12	2445	2443
717	383	30	-30	7	7	14	15	20	20	2479	2478
72.7	284	60	30	19	19	1.8	24	105	105	2602	2607
718						33		265	165		
	3.85	3.6	0	30	3 C 2 5		34	73		2800	2806
-720	366	3.0	-3C	25		29	2.2		73	2902	2901
721	387	6 C	1.5	34	34	22	29	187	167	3111	3117
728	388	3 C.	0	22	22	29	22	64	64	3204	3203
730	389	3.0	-3C	13	13	14	1.3	3.8	3.8	3256	3254
734	390	60	-15	5 C	5.0	19	28	275	275	3550	3557
735	35%	3 C	30	. z.	32	29	20	93	93	3672	3670
736	365	6 C	15	25	29	21	29	160	160	3853	3859
736	3 53	90	Ç	ê.	21	45	53	170	170	4C68	4082
?37	354	90	C	35	25	67	67	284	284	4419	44.32
737	395	30	-15	4	A	49	3.4	1.2	12	448C	4679
-738	396	3 €	-3C	11	1.1	14	1	3.2	32	4526	4525
744	357	3 C	Ç.	č	5	14	14	15	15	4555	4554
749	398	3 C	3 C	19	19	14	3.7	5.5	5.5	4624	4622
752	355	90	0.	14	14	32	4.8	113	113	4765	4783
767	400	3 C	15	22	22	48	32	64	64	4881	4879
768	401	6C	-15	13	13	21	29	72	7.2	4974	498C
77C	402	3 C	-30	7	7	29	21	20	2 C	5023	5021
771	403	30	3 C	13	13	14	13	3.8	3.8	5C75	5072
7.75	404	3€	30	E	6	14	14	1.7	17	5106	5103
784	405	90	0	28	2.8	31	4.7	227	227	5364	5377
-785	406	3€	45	19	C	45	C	55	C	5464	5377





Approved for	Release:	2025/06/18	C0513728
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	Approv	ed for Re	lease: 20	25/06/18	051372
3	31	23	23	5500	5431
1	28	105	105	5626	5564
9	22	41	41	5695	5627
9	26	77	77	5751	5730

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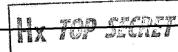
*			
-	HX	707	SECTION TO
			approximately a

			1				Approv	ed for Re	lease: 2	025/06/18	C05137282
165	467	3 C	-30	8	8	13	31	23	23	5500	5431
185	408	6 C	30	19	19	21	28	105	105	5626	5564
	409	3 C	15	14	14	29	22	41	41	5695	5627
perhan	410	60	15	14	14	19	26	77	77	5751	5730
	411	60	Č	30	30	32	32		165	5588	5927
	412							165			
	*	60	C	65	65	3.4	34	358	358	638C	6319
	413	6 C	15	22	0	34	C	121	C	6535	6319
100	414	6 C	15	24	24	34	36	132	132	6701	6487
800	415	3.0	-30	8	8	28	28	23	23	6752	6531
_801	416	3 C	15	7	7	14	13	2.0	2 C	6786	6564
301	417	3 C	-30	13	13	13	14	3.8	36	6837	6616
801	418	3 C	15	11	11	14	14	32	32	6883	6662
	419	3 C	C	8	8	15	14	23	23	6921	6659
301	420	6 C	15	35	35	23	32	193	193	71.37	6924
302	421	30	3.0	7	7	30	21	20	20	7187	6965
	422	30	-30	7	7	14	15	20	20	7221	7000
						15					
	423	6 C	-3C	29	29		27	168	168	7408	7195
315	424	3.0	15	19	19	27	8.1	55	55	7490	7268
	425	3 C	C	É	6	14	15	18	3.1	7522	7301
	426	3 C	3 C	28	28	14	13	81	81	7617	7395
	427	3 C	-3C	25	25	14	15	7.3	73	7704	7483
819	428	3 C	15	4	4	14	1.3	12	12	7730	7508
819	429	6 C	15	25	25	23	31	138	138	7891	7677
129	430	3 C	3 C	4	4	29	2.1	12	12	7932	771C
331	431	9.0	0	68	68	3.3	50	551	551	8516	8311
831	432	90	Č	16	16	7).	7 C	130	13C	8717	8511
-333	433	3 (-30	22	22	49	34	64	64	6830	86C9
333	434	3 C	-30	5	5	14	14	1.5	15	8859	8638
823	435	3 C	30	4	4	14	13	12	12	8885	8663
834				19	19	22	30	105	105	9012	8798
	436	60	15								
135	437	3 C	30	10	10	29	21	29	. 29	9070	8848
	428	3.0	-30	1.0	1.0	14	15	29	29	9113	8892
	439	6 C	-15	11	11	2.3	31	61	61	9297	6984
	44 C	3 C	30	2 C	TC	29	c 0	29	29	9255	9033
344	441	3 C	.30	43	43	13	14	125	125	9393	9172
	442	3 C	45	2.8	28	13	12	81	8.1	9487	9265
-347	443	90	.C	63	43	34	5-C	348	348	9869	9663
351	344	3 C	30	10	10	49	33	29	29	9947	9725
851	445	60	-15	20	20	24	33	110	110	10081	9368
	446	30	-30	12	12	3.0	2.2	35	35	10146	9925
	447	3 C	15	4	4	14	14	12	12	10172	9951
	448	3.0	-30	16	16	14	14	46	46	10232	10011
	445	3 C	3.0	8	8	1,6	14	23		10271	
	45C	30	-45	16	16	13	15	46			10109
	451	30	30	16	16	14	13	46		10390	
		30		7	7	14		20		10424	
	452		3.0				1.A				
-982		3 C	0	1.0	10	14	14	2.9		10467	
	454	90	0	35	3.5	3.3	50	284		10784	
	455		-15	50	5 C	69	69	405		11258	
_888	456	6 C	-30	C	8	C	51	C	44	11258	11148

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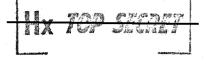
C051	L372	82				Appro	ved for R	elease: 2	2025/06/18	C0513728	2 818 00	ממת מנדו	1 74
111212121212121213131313131313131313131	07 60 07 30 09 30 10 30 11 30 12 30 14 120 15 30	150055505050 	9414693028	19 14 14 14 19 19 19 19 19 19 19 19 19 19 19 19 19	37 28 14 14 14 34 71 40	215431406551	119 1416 159 422 181	109 1161 416 429 422 422 123	14987 15134 15209 153264 153396 153396 16554 16675	14723 14723 14754 14913 14961 15975 16153	BIF-00	7/0-008	1-74
1027 1028 1028 1029 1029 1035 1044 1044 1044	17 60 18 60 19 60 20 30 22 30 20 20 20 20 20 20 20 20 20 20 20 20 20	0500000500 -330000500 -3100	21 55 55 47 17 17 51 10	21 35 47 17 17 51 10	21 45 12 14 14 14 14	29059459045 31122145	116 454 149 1406 94 171 29	193 142 206 49 171 29	17728 17948 18011 18126 18326 18369 18412	16398 16626 16787 17007 17071 17194 17385 17428			
1045655555555555555555555555555555555555	27 60 28 60 30 60 31 30 32 60 33 90 33 60 35 60 37 60	Seasonon and a	ZEZELLAZELA	44819012314	226658296777 3377	29 36 36 37 37 37 37	1375521218 1575521218 31768	154 171 55 332 121 72	19345 19726 19903 20012	18253 18327 18412 18801			,
1062 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	38 600 3200 340 300 3442 300 442 900 445 30	-30 35 35 35 35 35 35 35 35 35 35 35 35 35	1223 234462	12237034562	37 39 32 13 14 36 48 13	36 13 13 13 13 13 14 14 14 14 14 14	88 167 90 295 295 356 175	160 67 90 20 29 105 356 26	20429 20525 20628 20662	19498 19584 19687 19724 19764 19915 20335 20393 20424			
1077 5 1077 5 1077 5 1078 5 1078 5 1078 5	48 6C 49 6C 5C 3C 51 6C 52 6C 53 3C 54 5C	THE SHEET	262007175 101101175	36220017135	20 38 22 36 23 23 23 23 23 25 25 25 25 25 25 25 25 25 25 25 25 25	25 32 31 34 24 27 27	176 32 55 55 49 204 30 203	176 88 32 55 55 49 32 204	21609 21735 21796 21873 21964 22041 22086 2210 22428	2C677 2C8C1 2C855 2C941 21030 21099 21145 21376			

C0513	マ 7 フ 8 1	/											4
COST	,,	- ,				Approv	ed for Re	lease: 2	025/06/18	C05137282	BIF-0	07/D÷00	81-74
1 05C 55	7 60 -	-15	45	45	37	37	248	248	22713	2 781	**** *********************************		7
2090 55	8 30	3 C	13	13	29	20	38	3.8	2278C	21839			-
1092 55	9 90	0	62	62	34	5 C	502	50 Z	23316	22391	U.	TAB	San Lan San
: 93 56	0 30	3 C	7	7	48	32	20	20	23384	22443	ПХ	IUI	ed in the
1)93 56	1 30	15	7	7	13	13	20	20	23417	22476	~ ~ ~ ~		
1094 56	2 60	15	52	52	20	28	286	286	23723	22790			
1094 56	3 6C	15	15	19	36	36	105	105	23864	22931			
3 199 5£	4 3C	0	5	5	28	2.0	15	15	23907	22966			
1106 55	5 30	0	22	22	13	13	64	64	23584	23043			
11C6 56	6 3C	3 C	14	14	13	13	41	41	24038	23097			
1.06 56	7 30 -	-30	8	8	15	16	23	23	24C76	23136			
1.08 56	8 9C	0	37	37	34	49	300	30C	2441C	23485			
1109 56	9 6C	C	34	34	56	46	187	167	24653	23720			
1.09 57	0 30 -	-15	10	10	-28	21	29	29	2471C	23770			
1109 57	1 3C	15	8	8	14	14	23	2.3	24747	23807			
1169 57	2 3C	C	16	16	14	14	46	46	24807	23867			
3-09 57	3 3C ·	-3C	7	7	14	14	20	2 C	24641	23901			
.09 57	4 3C ·	-45	11	11	14	14	32	32	24887	23947			
1110 57	5 3C	3 C	19	19	14	13	55	55	24956	24015			
1110 57	6 6C	30	9	9	22	29	5 C	5 C	25C28	24094			
1.11 57	7 30 -	-15	65	65	29	23	187	188	25244	24305			

1208-4

B. CAMERA CPERATIONS SUMMARY REV 1111 OP 577 THROUGH REV 1694 OP 774

ĸEV	MSN	SCA	SCC	FRAN	r E S	INTE		PHOT	C-FT	CUM-TU	-FEET
Proc.	NUM			FNC	AFT		AFT	FHC	AFT	FWC	AFT
1_11	577	3 C	-15	13	13	0	C	36	35	36	35
1122	578	3 C	-30	14	14	77	77	41	41	154	153
1.22	579	3.0	3 C	24	24	14	13	70	7 C	238	236
1 .23	580	30	-30	14	14	14	15	41	41	293	292
1123	581	3 (30	11	11	14	13	32	32	335	337
1125	582	3 C	3 C	î C	2 C	14	14	29	29	382	380
.25	583	3 C	30	7	7	14	14	20	20	416	414
1126	584	60	15	28	28	21	29	154	154	591	597
1126	585	60	-15	13	13	35	36	72	72	698	705
7.30	586	3.0	Č	5	5	29	20	15	15	742	740
2.39	587	90	č	43	43	33	49	348	348	1123	1137
1141	5 8 8	90	0	34	34	67	67	275	275	1465	1479
7.41	589	3 C	-3C	21	Ž١	48	33	61	4.	1574	1573
.42	59C	30	-30	10	10	1.4	14	29	29	1617	1616
1142	551		-15	11	11	14	3.4	32	32	1663	1662
1442	592	30	-3C	9	9	14	1.3	26	26	1703	1761
142	553	3.0	-30	12	12	13	14	35	35	1751	1750
1142	554	3 C	C	7	7	14	13	20	žć	1785	1783
1148	595	5 C	-15	22	22	20	28	121	121	1926	1932
7.48	596	3 C	-15	8	8	29	21	23	23	1978	1976
.55	597	60	3.0	7	7	21	28	39	39	2038	2043
11.55	598	6Ĉ	Ō	16	16	36	36	8.8	8.8	2162	2167
₹57	599	3 C	-15	13	1.3	2.8	21	38	36	2228	2226
	600	3.0	-3C	12	12	14	14	35	35	2277	2275
1158	601	6.C	15	26	26	21	2.8	143	143	2441	2446
1158	6 C 2	6.0	C	13	13	36	3.7	72	7.2	2549	2555
158	603	26	3 C	4	4	28	19	1.2	12	2589	2586
.159	604	60	15	5 C	50	21	29	275	275	2665	2890
1164	€ C 5	60	-15	10	" C	33	34	55	55	2973	2979
1,67	606	60	15	19	19	32	3 C	1,05	2 C 5	3109	3114
159	607	3.0	٥	10	10	25	13	29	29	3163	3161
1165	833	3 C	15	11	11	13	12	32	32	3208	3205
-169	609	3 C	-3C	E	5	13	14	15	1.5	3236	3234
1.71	ELC	60	-15	10	10	20	28	55	55	3311	3317
1171	611	6 C	-15	24	34	3.5.	35	187	187	3,533	3539
1171	612	é C	15	7	7	37	36	3 9	35	3609	3614
172	613	6 C	15	6	É	36	36	3 3	33	3678	3683
£174	614	6 C	-15	4	4	35	36	2.2	22	3735	3741
1174	615	3.0	C	19	19	27	18	55	55	3817	3814
174	616	6 C	-15	14	14	20	30	77	7.7	3514	3921
174	617	3 Ç	C	8	d	25	ZΟ	2.3	23	3966	3964
1180	618	30	-30	26	26	13	13	75	75	4 C 5 4	4052
-180	615	3 C	-30	11	11	14	14	32	3.2	41CC	4098





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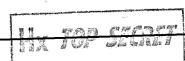
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2 81	353	3 C	15	5	5	14	23	1.5	15	4129	4126
1183	621	3 C	30	22	22	13	13	64	64	4206	4203
1-87	622	6 C	3.0	19	19	19	27	1.05	105	4330	4335
: .87	623	6 C	15	2.5	25	35	35	138	138	4503	45C8
1187	624	60	0	1 C	1.0	36	36	55	55	4594	4599
1189	625	6 C	0	16	16	35	35	88	8 8	4717	4722
1.90	626	60	-15	27	27	34	3.5	149	145	490C	4906
1.90	627	6 C	3 C	13	13	35	34	72	72	5007	5012
1190	628	6 C	-15	4	4	36	37	22	22	5065	5C71
.91	629	96	a	74	74	47	54	599	599	5711	5724
: 203	630	6Ċ	15	10	î, C	54	46	55	55	5820	5825
1207	631	60	0	7	7	36	37	39	39	5895	5901
-218	632	3.0	C	.5	5	29	21	15	15	5939	5937
220	633	6 ¢	-15	15	19	20	27	105	165	6064	6069
1221	634	60	-15	11	11	32	3.3	61	61	6157	6163
1221	635	6.0	Ċ	7	7	33	3.2	39	39	6229	6234
223	636	60	3 C	19	19	3.5	34	105	105	6365	6373
23c	6.3.7	9.0	0	10	10	46	55	81	21	6496	6509
1236	638	60	15	25	25	54	46	138	138	6688	6693
237	635	6¢	15	16	16	36	36	8.8	9.8	6812	6817
245	640	60	15	1 C	10	36	36	55	55	6903	6908
1300	641	60	C	6	6	79	39	33	3.3	7C15	6980
3-30C	642	60	15	19	C	35	¢	105	C	7155	698C
302	643	3 C	-45	29	29	29	20	84	84	7268	7084
1302	644	9 C	15	22	22	34	49	178	178	748C	7311
1303	645	60	30	13	13	55	46	72	72	76C7	7429
30.3	646	6 C	-15	1 C	10	35	3.6	55	55	7697	7520
.363	647	60	15	22	22	3.6	36	121	121	7854	7577
46 46 46 4		~ *		4. 75	46.775		P	4.7		-000	4 6 6 6



Approved for Release: 2025/06/18 C05137282

.C0	513	7282				Appro	ved for F	Release:	2025/06/18	3 C05137282	RIELOO	7/D <u>-</u> 008	L-74
1 136	670	30 1	5 5	5	29	20	15		11681		D11-00	77 D-000	1 - 7 +
1348	671	60 -19	5 14	14	20	29	77		11778				×10x 227 ×
1349	6.72	6C -1	5 13	13	37	37	72	72	11887	11709	11	TAD	CENT
149	673	6C (0 25	25	37	37	138	135			TIA	1 40	DEV SIGN TO
1.350	674	6C -19	5 29	25	36	37	160		12258				
1351	675	6C 1	5 16	16	37	36	88		12383		1		
364	676	30 -30	9	49	28	21	142			12368			
: 165	677	9.0	0 31	31	34	49	251	251	12838	12668			
1366	678	90 (73	73	67	67	591	591	13496	13326			
.—166	679	9C (11	11	68	68	89	89	13653	13483			
167	68€	30 30	45	45	48	32	131	131	13832	23646			
1368	681	60 1	5 25	25	22	29	138	138	13992	13813			
1365		6C 1	5 89	E 9-	36	37	490	49¢	14518	14340			
374		3C 31	17	1.7	29	21	49	49	14596	14410			
1375			3.8	3.6	21	29	209	209	14826	14648			
1382	685		22	22	48	5.6	178	178	15C52	14882			
. 382	686	6C 1		21	57	45	116		15225	15047			
383	687	6C -19	5 14	14	36	37	7.7	7.7	15338	15161			
1383	688	60 -15	5 13	13	37	3.7	72	72	15447	15270			
-184	669	6C 1	5 3 C	3 G	37	36	165	165	15649	15471			
185			87	87	48	56	7.05		16402	16232			
1397	691	6C -1	5 14	14	56	4.8	77			16357			
1397		6C (2 15	15	37	37	83	8.3	16655	16477			
399	6.93	3C -30		13	29	22	38	38	16722	16537			
a400		60 -1		15	2.2	3 C	83		16827				
1401	695	60 -15		13	3.8	37	72	72					
101	696	30 30	33	33	29	21	96		17062				
ACL	697	3C 1		9	15	15	26		17103				
1402	698	6.C 19	5 17	17	٤ŝ	30	94		1722C				
1413	695		3E C	36	45	54	308			17403			
415		60 1		£ 6	50	42	143		17766				
1416	701	6C -1!		9	33	34	5 C		17849				
1417	702		34	3.4	44	51	275		18168				
122	7 C 3	3(-3)		Ş	45	3.0	2.0		18239				
429	704		54	54	31	45	437		18707				
1430	7 C 5		5.0	ž C	66	6.6	405	405	19178				
7437	766	60 X		3 C	54	46	165		19397				
431	707		5	5	27	19	15	15	19439				
1433	708		5 9	G:	20	31	50		19509				
445	709		34	34	45	5.2	275	275	19829				
445	710	6C -15		1.3.	53	45	72	72	19954				
1449	711	60 31		9.	35	34	50		20039				
1462	712		3 13	13	3.6	36	72	72					
456	713	60 15		17	34	34	94		20275				
z 466	714	1 1-4	5	9	35	3.5	50			20183			
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1 27	720	6 C	-15	14	14	22	31	77	77	21037	20861
1497	721	3·C	-3C	13	13	29	21	38	3.8	21164	20920
7-33	722	30	-30	12	12	14	14	35	35	21153	20969
1 11	723	6 C	C	13	1.3	21	28	72	7.2	21246	21069
1515	724	30	-15	Ģ	9	2.8	21	26	2.6	21300	21116
1515	725	3 C	15	25	25	13	12	73	73	21386	21201
1 31	726	ó C	15	36	36	21	28	198	198	21605	21427
1335	727	3 C	-30	25	25	28	21	73	73	21706	21521
		30	-30	īí							
1536	728				11	13	14	32	32	21751	21567
136	729	6 C	15	3 C	10	2.2	29	55	55	21828	21651
146	730	.6€	-15	21	21	36	37	116	116	21980	21804
1547	731	3 C	C	15	15	28	20	44	44	22052	21868
.º552	732	.3 C	C	6	6	14	14	18	1.8	22C84	21900
354	733	3 C	C	8	8	14	14	23	23	22121	21937
1559	734	60	-15	47	47	21	29	259	259	22401	22225
156C	735	3 C	3.0	ç	9	30	20	26	26	22457	22271
551	736	3 C	-15	5	5	13	15	15	15	22485	223C1
1,562	737	60	0	19	19	20	27	105	105	22610	22433
1563	738	90	0	3 C	3 C	45	54	243	243	22898	22730
36€	739	6 C	-15	19	19	5.5	47	105	105	23058	22882
559	74 C	3 C	-30	7	7	29	21	20	20	23107	22923
1570	741	100 000	1.00	g	ģ	22	29	50	5 C	23179	23002
*575	742	60	0	22	22	26	36	121	121	22326	23159
576	743	3 C	C	46	46	28	20	133	133	23487	23312
1577	744	3 C	3 C	19	19	13	13	55	55	23555	23380
1535	745	3 C	Ö	6	6	13	13	1.7	17	23585	2341C
592	746	30	3.0	23	2.3	14	14	67	67	23666	23491
4395	747	3.0	3.0	3 C	3 C	1.4	14	87	87	23767	23592
1596	748	3 C	30	2.3	23	13	13	67	67	23847	23672
557	749	30	15				15	15	15	23877	237C2
				5	5	15					
507	75C	3 C	-30	58	5.8	13	14	168	168	24058	23884
1610	751	60	15	21	21	21	28	116	ilt	24195	24 C Z 8
2012	752		· C	7.8	7.8	47	55	632	632	24874	24715
617	753	3.0	3.0	1.2	12	4.8	32	3.5	35	24957	24782
1626	754	6 C	C	22	12	21	25	6.6	66	25044	24877
1428	755	90	- 25	3.7	22	48	57	178	178	25270	25112
643	156	3.0	15	6	6	50	33	1.7	1.7	25337	25162
2633	757	30	.a. 2	6	6	13	13	27	1.7	25367	25152
1635	758	3.0	-15	. 5	5	13	14	1.5	15	25395	25221
~64 L	755	6 C	-15	ĺć	16	17	25	83	3.9	25500	25334
657	76C	30	30	1.3	13	29	20	38	38	25567	25392
1657	7.61	3 C	1,5	8	8	14	15	2.3	23	25604	25430
1 -658	762	60	-15	14	14	2 Z	3 C	77	77	25703	25537
	763	30	-15	7	7	29	21	20			25578
1667			15	5	5	14	14	15		25781	
1673			-15								
A 1 1 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	3 C D			12	12	21	29	66		25868	257CZ
677	155	60	Û	15	15	37	36	83		25588	25821
.678			-3C	5	5	28	22	15	15	26C31	25857
1689			3.0	C	30	C	13	G		26031	
Tésc	765	3 C	-15	1.5	19	14	14	55	55	261CC	26026

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			_		-			-				
1893 771	6C C	1	7	22				26204				
1693 772	3C -30	9	9:	28	21	26	26	26258	26184	LI.	TADA	CCCOCK
193 773	SC C	15	15	36	51	122	122	26416	26357	HIX	101	JA CINE I
_394 774						185	167	26658	26573	1		
				32	62			26690	26635	-		Mg/HAMMen-
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